Technical Memorandum



To: Mr. David Kepler

Mr. Ron Hansen, P.E., P.S.

From: Paul D. Drew, P.E., CFM, Richard J. Anderson, P.E., William H. Walton, P.E. (MI), S.E.

Date: July 13, 2020

Re: Post Failure – Reconstruction Cost Analysis

Four Lakes Task Force (FLTF)

Midland, Michigan

GEI Project No. 2002879

Introduction and Project Background

This technical memorandum (TM) presents the results of a study by GEI Consultants of Michigan, P.C. (GEI) to develop "planning-level" opinions of probable construction cost to reconstruct and/or rehabilitate the four hydropower dams currently owned by Boyce Hydro, LLC (Boyce), Sanford, Edenville, Smallwood, and Secord (list from downstream to upstream), following the May 19, 2020 flood that resulted in severe damage to the Smallwood Dam and a catastrophic failure of both the Edenville and Sanford Dams. No obvious visual damage has been reported by Spicer Group Inc. (SGI) at Secord Dam. In response to the failures, the Federal Energy Regulatory Commission (FERC) ordered that the current owner (Boyce Hydro) to:

- 1) Safely draw down the impoundment of each of the four dams,
- 2) Have an independent engineer inspect each of the four dams,
- 3) Develop an interim plan to safely pass flows until a safe reservoir elevation can be established and implemented, and
- 4) Engage an independent panel of experts to perform a root cause forensic evaluation of the dam failures.

Furthermore, we understand that Gladwin and Midland Counties have signed a resolution in June 2020 to have the four projects condemned in accordance with Part 307 of the Michigan Natural Resources and Environmental Protection Act (NREPA).

GEI has not yet received permission to access the sites to perform a visual assessment of the dams, and inspection reports by an independent engineer have not yet been provided to us. Therefore, the opinions of probable construction cost presented in this TM are solely based on engineering judgement and expert opinion based on our experience with the design and construction of similar dams. We understand these planning level costs will be used by the County's assessors to estimate the current value of the assets and liabilities associated with acquiring the properties from Boyce. Since we have not had an opportunity to inspect the dams following the failures and because FERC has ordered Sanford, Smallwood, and Secord Dams to be fully drawn down, we assume that none are currently safe to retain and pass ½ probable maximum flood (PMF) water flows and will either need complete reconstruction (Sanford and Edenville Dams) or major rehabilitation (Smallwood and Secord Dams). Prior to the May 2020 flood event, a number of significant dam safety deficiencies, including insufficient spillway capacity to pass the design flood event, were identified by the previous Part 12D Independent Consultant D. Purkeypile, P.E., the

FERC and the Michigan Department of Environment, Great Lakes and Energy (EGLE) that needed to be addressed to bring the dams into compliance with State and Federal guidelines.

Criteria for Developing Opinions of Probable Construction Cost

The engineers' opinions of probable construction cost presented in this TM assumes the following criteria for the complete reconstruction of the Sanford and Edenville Dams, and the rehabilitation of the Smallwood and Secord Dams:

- The reconstruction / rehabilitation of the four dams will provide 75+ year design service life.
- The reconstruction / rehabilitation of the four dams will be designed to meet the current industry standards of engineering practice and the design standards for high hazard dams in accordance with the Michigan Department of Environment, Great Lakes and Energy (EGLE).
- Restoring hydropower generation would not be part of the reconstruction and was not included in our costs.
- The spillways for all four dams will be required to safely pass ½ of the Probable Maximum Flood (PMF) in accordance with the current State of Michigan EGLE dam safety requirements. A separate set of cost estimates was developed presuming the dams would be reconstructed to pass the full PMF per FLTF's request.
- A means to substantially draw down each of the four impoundments (i.e., add or enhance low level outlets).
- The ability to safely pass base plus flood flows (assumed 100-year storm event) without failing during construction.

Data Review

The information collected and used to develop an engineer's opinion of probable construction costs includes the following:

- Sanford, Edenville, Smallwood and Secord Design Drawings, 1923 to 1924.
- Sanford, Edenville, Smallwood and Secord Dam Improvement Drawings, SGI, 2020.
- Supporting Technical Information Document (STID), Sanford, Edenville, Smallwood and Secord.
- Probable Maximum Flood Upgrades, Secord Dam FERC Project No. 10809, GEI Consultants, April 2020.
- DRAFT Discharge Rating Curves (Secord, Smallwood, Edenville and Sanford Projects), GEI Consultants, April 2020.
- DRAFT Probable Maximum Flood Determination, Ayers Associates, May 2020.
- Post Failure Drone Photographs provided by SGI, May 2020.
- Unit price cost data from various dam repair / reconstruction projects within the last five (5) years (ref. GEI project records from similar projects)

Hydrology and Hydraulics – Existing Conditions

Ayers Associates under contract to the SGI, performed an updated PMF study in May 2020 to re-evaluate the PMF at all four projects using improved precipitation, streamflow and watershed data in accordance with current FERC engineering guidelines. The Four Lakes Task Force (FLTF) requested that GEI review the available hydraulic information and develop new spillway discharge rating curves for each project. The updated spillway rating curves were provided in the GEI April 2020 Technical Memorandum and submitted to Ayers for their use in the PMF study update. As shown in **Table 1**, the results of the Ayers

PMF study indicate the each of the four projects lack the necessary spillway capacity to safely pass the PMF.

Table 1:	PMF Flood Routing – Existing (Pre-May 2020 Flood) Conditions
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Dam	Peak PMF Inflow (cfs)	Peak PMF Outflow (cfs)	Peak Reservoir El. (ft)	Min. Dam Crest El. (ft)	Overtopping (ft)
Secord Dam	29,400	$28,100^{1}$	759.0	757.8	1.2
Smallwood Dam	41,200	41,000	716.8	715.7	1.1
Edenville Dam	80,900	80,100	686.0	682.1	3.9
Sanford Dam	$80,600^2$	79,100	641.2	636.8	4.4

Notes:

- 1. Includes 13,000 cfs flowing over the east reservoir rim private home and properties and into the Tea Creek Drainage Area.
- 2. Sanford Dam Inflow Design Flood (IDF) = 37,000 cfs
- 3. Elevations (El.) listed herein are referenced to the National Geodetic Vertical Datum of 1929 (NGVD29).

Description of Existing Project Facilities

The Sanford and Edenville Dams breached on May 19, 2020 after several days of intense rainfall. Smallwood Dam incurred significant damage due to high flows and resulting scour erosion of the embankments. The damage to Secord Dam is uncertain, but SGI reported no significant damage was visible from visual observations. FERC in their letter dated May 20, 2020 to Boyce Hydro, ordered Boyce to full drawdown the impoundments behind all four dams. We understand that several of the water retaining structures, including the Edenville embankment to the west of the Michigan highway M-30 causeway and the Tobacco River Spillway, are still impounding some amount of water since no low-level outlet is present to fully draw down the impoundments. The Sanford embankments and fuse plug spillway are completely breached but the spillway and powerhouse structures are still standing. The amount of damage to the remaining structures is uncertain since GEI has not yet received permission to access the sites to perform a visual assessment of the dams and post-failure inspection reports by others have not yet been provided. However, it is our assumption that given the damage to the adjacent structures, depth and quantity of flood flow and observations from drone footage, that existing powerhouse and spillways at both Edenville and Sanford Dams are assumed to have incurred significant damage to their abutments and potentially undermining and toe erosion downstream of the structures.

We developed a "high-level" list of reconstruction and rehabilitation activities anticipated for the water retaining structures at each dam. These repairs or reconstruction activities are based on available design drawings, previous condition reports, previous engineering studies, and post-flood condition assessment records provided by SGI including post-failure photos and drone videos. The following lists the general condition of the gated spillways, powerhouses and embankments observed at each of the four dams. **Table 2** provides a summary matrix of the major reconstruction and rehabilitation items likely needed at each of the four dams. Photographs of the condition of the four dam's post-failure condition are provided in **Attachment 1**.

Based on our review of the information provided to date, we have assumed the following for the purposes of estimating reconstruction and repair costs:

Existing Gated Spillways:

• None of the four dams meet FERC engineering standards for spillway discharge capacity (full PMF) or residual available freeboard (i.e., all embankments overtop). Only Smallwood Dam has sufficient spillway capacity to meet the Michigan EGLE's flood capacity requirements (1/2 PMF).

- The gated spillways are reinforced concrete hollow, buttress-type structures constructed on soil that were more common pre-1940s when materials were expensive and labor cheap. This style of dam does not currently meet industry standards of design practice in terms of long-term durability and ductility during an earthquake.
- The projects do not include sufficient downstream energy dissipation structures or armor stone or riprap to protect against high tailwater and velocities that can scour un-zoned earth dam toes and spillway abutments.
- Edenville and Sanford spillways may have been shifted or undermined during the May 2020 flood. Status of tailrace scour and undermining at the Smallwood and Secord Dams is uncertain.
- Existing concrete spillways at each of the four projects were constructed on non-air entrained concrete and exhibit extensive deteriorations.
- The existing Tainter gates are likely beyond end of their design life and exhibit signs of age and corrosion. The Tainter gate hoisting mechanisms are generally insufficiently sized for the range of design service loads including ice and do not meet current industry design standards for wire rope cable hoists and several automated gate operators.

Existing Powerhouses:

- The amount of potential downstream scour, undermining and damage to the Sanford and Edenville Powerhouses is uncertain. The Sanford and Edenville Dams will likely need to be demolished and excavations made to sound foundation soils within dry cofferdams.
- The projects will need to include low-level outlets at all of the dams as a means to partially drain or draw down the impoundment. The powerhouse draft tubes could be converted to low-level outlets at Smallwood and Secord Dams and filling the remaining passages with mass concrete. However, if the hollow areas under the rollway slabs and between the piers are filled in with lightweight grout or concrete (heavier than water), the powerhouses would likely require underpinning with grouted steel micro-piles founded in native soil to prevent settlement and cracking under the additional weight of concrete fill.
- The water passages at the Sanford and Edenville powerhouses are not large enough to serve as a low-level outlet without the risk of reservoir refilling for events up to the 100-year flood.

Existing Embankments:

- None of the embankment dams were constructed to modern standards since they are homogenous (un-zoned), contain no impervious core or seepage cutoff, no internal filter sand and gravel drainage system, insufficient upstream erosion protection and are all generally too steep. Only the Smallwood Dam embankment has a sheet pile seepage cutoff through the dam into the foundation.
- The embankment dams at Secord and Edenville will need to be completely reconstructed including installation of a fully penetrating dam into foundation seepage cutoff wall, downstream granular filter sand / drainage gravel zones to control dam and foundation seepage that bypasses the cutoff, downstream slopes flattened or stabilized to improve stability, and installation of armor stone riprap and bedding to prevent erosion along the upstream face of the dam during high flows.
- Extensive damage or complete failure observed at all embankments except at the Second Dam.

Table 2: Matrix of Major Dam Reconstruction Items

Reconstruction Item	Sanford	Edenville ¹	Smallwood	Secord
Abutment Reconstruction / Laydown Area	V		Ø	Ø
Water Diversion During Construction	V	QQ	Ø	Ø
Powerhouse Decommissioning/Demo	V		Ø	Ø

Reconstruction Item	Sanford	Edenville ¹	Smallwood	Secord
Existing Gated Spillway Demolition	V	QQ	NA	NA
Repair Existing Gated Spillway	NA	NA	Ø	Ø
New Gated Spillway		V	NA	NA
New Auxiliary Spillway		QQ	Ø	Ø
Left Embankment Reconstruction		QQ	NA	NA
Right Embankment Reconstruction		QQ	NA	NA
Left Embankment Repair	NA	NA	Ø	Ø
Right Embankment Repair	NA	NA	Ø	V
U/S and D/S Cofferdams		QQ	Ø	Ø
U/S and D/S Channel Restoration		QQ	Ø	Ø
Regrading and Erosion Control	$\overline{\mathbf{A}}$	QQ	Ø	Ø
Temporary M-30 Diversion Structure	NA	Ø	NA	NA
Grouted Micro-piles and Underpinning	NA	NA	Ø	Ø
Regrading and Erosion Control	V	QQ	Ø	V

Notes:

- Two check boxes to denote required at both the Edenville and Tobacco spillways and flanking earthen embankments because the
 dams were constructed at the confluence of the Tobacco and Tittabawassee Rivers and need to manage flows past them
 independently.
- 2. NA Not applicable

Description of Proposed Project Repairs

Based on the condition of the existing project facilities, GEI has developed new conceptual spillway and dam configurations for each of the four projects which would allow the four dams to safely pass the ½ PMF. The configurations consist of reconstruction or rehabilitation of earthen embankments, demolition and replacement of the primary gated spillways, low-level outlets, powerhouse demolition / abandonment, and construction of new passive auxiliary spillways. Conceptual-level proposed spillway rating curves (see **Attachment 2**) were developed using the methods prescribed in the United States Bureau of Reclamation Design of Small Dams (USBR) 1987) and Hydraulic Design of Labyrinth Weirs – Henry T, Falvey (Falvey 2003). The following list the general dam configurations and preliminary flood routing of each of the four projects.

Sanford Dam:

The Sanford Dam gated spillway and powerhouse will be demolished and replaced in the same location with a slightly wider and deeper spillway. The spillway ogee shaped crest will be constructed at El. 620.0 with six (6) 22-foot wide automated Obermeyer or hydraulic crest gates to increase spillway discharge capacity. One (1) of the gates will be a deep gate installed at a lower sill elevation to provide a means to draw down the impoundment. The automated gates would be designed to open and close with minimal human intervention during normal operation and flood events. Operation of the crest gates would remain the primary means for regulated releases through the impoundments under normal operations and flood conditions. The proposed spillway structure will discharge through a rectangular spillway chute and USBR type stilling basin.

A new 165-foot-wide, minimum 6-cycle auxiliary labyrinth spillway structure (see Figure 1) will be constructed at weir El. 632.5 within the right embankment near the footprint of the existing breach channel to provided additional spillway capacity during the ½ PMF. The labyrinth spillway will have an un-gated passive overflow crest that will control water surface elevations during extreme flood events without human intervention.

The Sanford Dam embankments will be reconstructed to minimum El. 638.0 feet to provide adequate freeboard for all inflows up to and including the ½ PMF. The downstream slopes will be constructed to 2.5H:1V to provide adequate stability in accordance with EGLE stability requirements under normal and flood pool loading criteria. A new permanent steel sheet pile cutoff (PZC-26 or equal hot rolled sheets with interlock sealants) will be constructed upstream of the dam crest and extend into the impermeable clay till foundation soil to provide a seepage barrier cutoff. Downstream granular filter drainage layers will be constructed to control seepage that bypasses the cutoff. The downstream slope will be buttressed and armored with new riprap and bedding material to protect against high tailwater flood conditions. The upstream slopes will be protected from beaching and wave erosion by the installation of bedding and riprap sized for fetch and wave runup. A minimum crest width of 20 ft will be provided to access the dam and spillways. Typical Sanford Dam embankment reconstruction is provided in **Figure 2**. Preliminary flood routing is provided in **Table 3**.

Table 3: Sanford Dam ½ PMF Flood Routing – Proposed Conditions

Peak ½ PMF Inflow (cfs)	Primary Spillway Discharge (cfs)	Auxiliary Spillway Discharge (cfs)	Total Spillway Discharge (cfs)	Peak Reservoir Stage (ft)	Design Dam Crest (ft)	Freeboard (ft)
40,300	33,235	7,835	40,945	636.0	638.0	2.0

Notes:

- 1. Construct new primary spillway with six (6) new 22-foot wide crest gates at El. 620.0 ft (lowered from El. 622.3)
- 2. Raise the Embankments from El. 636.8 to El. 638.0 ft
- 3. Construct new labyrinth spillway at El. 632.5 ft

Edenville Dam:

The Edenville and Tobacco gated spillways and powerhouse will be demolished and replaced in the same location with slightly wider and deeper spillways independent of each other in the long-term to allow the Tobacco and Tittabawassee Rivers to maintain their drainage and tailrace ecosystem upstream of their natural confluence. The improved Edenville and Tobacco ogee crests will be installed at El. 665.5 with three (3) 24-foot wide Obermeyer or hydraulic crest gates to increase spillway discharge capacity. One (1) of the gates will be a deep gate installed at a lower sill elevation to provide means to substantially draw down the impoundment. The automated crest gates would be designed to open and close with minimal human intervention during normal operation or during flood events.

New 125-foot-wide, 6-cycle auxiliary labyrinth spillway structures (see Figure 1) will be constructed within the Tobacco and Edenville embankments impounding the Tobacco and Tittabawassee Rivers respectively, at El. 677.8 to provided additional spillway capacity during the ½ PMF. The proposed spillway structure will discharge through a rectangular spillway chute and USBR type stilling basin.

Similar to the Sanford Dam, the Edenville and Tobacco earthen embankments will be fully reconstructed to provide adequate freeboard for all inflows up to and including the ½ PMF. The typical Edenville embankment reconstruction is provided in **Figure 2**. Preliminary flood routing is provided in **Table 4**.

Peak ½ PMF Inflow (cfs)	Primary Spillway Discharge (cfs)	Auxiliary Spillway Discharge (cfs)	Total Spillway Discharge (cfs)	Peak Reservoir Stage (ft)	Design Dam Crest (ft)	Freeboard (ft)
40,450	30,615	10,720	41,335	681.0	685.0	4.0

Table 4: Edenville Dam ½ PMF Flood Routing - Proposed Conditions

Notes:

- Construct new Edenville primary spillway with three (3) new 24-foot wide crest gates at El. 665.5 (lowered from El. 667.8) for the Tittabawassee River.
- Construct new Tobacco primary spillway with three (3) new 22-foot wide crest gates at El. 665.5 (lowered from El. 667.8) for the Tobacco River.
- 3. Raise the embankments from El. 682.0 to 685.0.
- 4. Construct new 125-foot wide Edenville labyrinth spillway at El. 677.8 for the Tittabawassee River.
- 5. Construct new 125-foot wide Tobacco labyrinth spillway at El. 677.8 for the Tobacco River.

Smallwood Dam:

The Smallwood Dam gated spillway will be repaired and the two (2) existing Tainter gates will be replaced with either automated Obermeyer or hydraulic crest gates. The powerhouse will be decommissioned, and the draft tubes converted to low-level outlets and the remaining passages filled with mass lightweight grout or concrete. The filled-in powerhouse will likely require underpinning with grouted steel micro-piles founded in hardpan clay to minimize excessive settlement and cracking under the additional weight in the voids of the powerhouse.

Currently the Smallwood Dam has sufficient capacity to pass the ½ PMF through the spillway gates and existing auxiliary spillway. However, an auxiliary spillway will likely be needed to pass base and flood flows during the rehabilitation of the existing gated spillway and powerhouse. A new passive, 125-foot-wide, minimum 6-cycle, reinforced concrete auxiliary labyrinth spillway structure will be constructed at El. 709.5 within the left embankment to pass base flows during construction and provide additional spillway capacity during the ½ PMF. The proposed spillway structure will discharge through a rectangular spillway chute and USBR Stilling basin (see Figure 3).

The Smallwood embankment slopes will be flattened to a minimum slope of 2.5H:1V to provide adequate stability in accordance with EGLE stability requirements under normal and flood pool loading criteria. The embankment toe and downstream slope was damaged and eroded during the May 2020 storm and will be repaired with new structural fill and buttressed with new riprap and bedding stone. A minimum crest width of 20 ft will be provided to access the spillways. The upstream slope will be protected with riprap over bedding stone. A typical Smallwood dam embankment repair section is provided in **Figure 4**. Preliminary flood routing is provided in **Table 5**.

Table 5: Smallwood Dam ½ PMF Flood Routing – Proposed Conditions

	Peak ½ PMF Inflow (cfs)	Primary Spillway Discharge (cfs)	Auxiliary Spillway Discharge (cfs)	Total Spillway Discharge (cfs)	Peak Reservoir El. (ft)	Design Dam Crest El. (ft)	Freeboard (ft)
ĺ	20,600	13,380	7,500	20,880	713.5	715.7	2.2

Notes:

- 1. Remove Tainter gates and replace with crest gates at invert El. 694.8
- 2. Construct new 125-foot wide labyrinth spillway at El. 709.5

Secord Dam:

The Secord Dam gated spillway will be repaired and the two (2) Tainter gates will be replaced with automated Obermeyer or hydraulic crest gates at El. 737.5 to increase spillway capacity. The powerhouse will be decommissioned, and the draft tubes converted to low-level outlets and the

remaining passages filled with lightweight grout or mass concrete. The powerhouse will likely require underpinning with grouted steel micro-piles founded in hardpan clay to reduce settlement.

As documented in the Preliminary Design Basis Report by GEI in April 2020, a significant portion of the inflow into Secord Lake discharges over the populated (e.g., with streets, homes and yards) Secord Lake Ridgeline and left abutment rim at El. 755.0 into Tea Creek before reaching the dam. This overflow presents a significant flood risk to the resident's homes and streets along the eastern shoreline of Secord Lake. The goal of this proposed configuration is to pass the ½ PMF without surcharging the reservoir above the Secord Lake Ridgeline at El. 755.0 and reduce flood impacts to the eastern shoreline residential properties including streets, utilities, homes and yards.

A new 200-foot-wide ungated, reinforced concrete overflow spillway will be constructed at El. 752.0 to provided additional spillway capacity during the ½ PMF. Conceptually, the spillway would consist of a passive concrete overflow weir, concrete chute, stilling basin and discharge channel to the Tittabawassee River (see **Figure 5**). The spillway will have an un-gated passive overflow crest that will control water surface elevations during extreme flood events without human intervention. Operation of the crest gates would remain the primary means for regulated releases through the impoundments under normal operations and flood conditions.

The Secord Dam embankment slopes will be flattened to provide adequate stability in accordance with EGLE stability requirements under normal and flood pool loading criteria. A new permanent steel sheet pile cutoff (PZC-26 hot rolled sheets with interlock sealants) will be constructed upstream of the Secord dam crest and extend into the clay till to provide a seepage cutoff. New drainage filter and drainage stone will be constructed along the interface of the existing downstream slope and new embankment fill. Lastly, the downstream slope will be buttressed with new riprap and bedding material to protect against high tailwater flood conditions. A typical Secord embankment repair section is provided in **Figure 6**. Preliminary flood routing is provided in **Table 6**.

Table 6: Secord Dam ½ PMF Flood Routing – Proposed Conditions

Peak ½ PMF Inflow (cfs)	Primary Spillway Discharge (cfs)	Auxiliary Spillway Discharge (cfs)	Total Spillway Discharge (cfs)	Peak Reservoir Stage (ft)	Design Dam Crest (ft)	Freeboard (ft)
14,700	11,470	3,430	14,900	755.0	758.0	3.0

Notes:

- 1. Lower existing spillway gate sill from El. 742.8 to El. 737.5 to increase spillway capacity
- 2. Replace Tainter gates with two (2) new crest gates
- 3. Construct 200-foot wide passive overflow spillway structure at crest El. 752.0

Construction Sequence and Considerations

The proposed project configurations will require the ability to route base river flow and storm flows through each dam and divert flows around the construction work areas throughout the duration of the construction projects. Because the construction duration will last multiple years, the project will require significant upstream and downstream cofferdams and flow diversion. Upstream and downstream temporary cofferdams will be required to allow demolition of the powerhouse and existing gated spillways, and construction of the new gated and auxiliary spillways. The proposed cofferdams will likely consist of 35- to 40-foot-diameter sheet piles comprised of PS-27.5 sheets filled with granular fill that are self-stable under the range of anticipated hydraulic and ice loads during construction. The upstream cofferdam will be constructed above 100-year flood elevation during construction to provide adequate freeboard during construction. Typical Cofferdam plans for Sanford and Edenville Dams are provided in **Figure 7** through **Figure 10**. The anticipated

construction sequence for the four projects starting at Sanford Dam and working upstream towards Secord Dam is as follows:

Sanford Dam

- 1. Fully draw down impoundment, stabilize existing project structures, remove debris and inspect spillway and powerhouse. (To be completed by Boyce)
- 2. Contractor mobilization, left and right abutment reconstruction and develop laydown and contractor work areas.
- 3. Stabilize right embankment breach channel and fully divert water from spillway and powerhouse area.
- 4. Construct Phase I upstream and downstream cofferdams at gated spillway and powerhouse.
- 5. Demolish existing gated spillway and powerhouse.
- 6. Construct new gated spillway.
- 7. Remove Phase I cofferdams and construct Phase II upstream and downstream cofferdams at new auxiliary labyrinth spillway located at breach channel area. Divert river flows through new gated spillway.
- 8. Construct new auxiliary labyrinth spillway and reconstruct flanking embankments.
- 9. Remove Phase II cofferdams.
- 10. Refill Sanford Lake and, monitor performance.
- 11. Final site restoration and contractor demobilizations.

Edenville Dam

- 1. Fully draw down impoundment, stabilize existing project structures, remove debris and inspect spillway and powerhouse. (To be completed by Boyce).
- 2. Contractor mobilization, left and right abutment reconstruction and develop laydown and contractor work areas.
- 3. Improve and stabilize diversion through left embankment breach channel.
- 4. **Construct temporary diversion control structure at M-30 bridge upstream of Tobacco Dam to allow partial flow of either river (Tittabawassee or Tobacco) to either watershed.**
- 5. Construct Phase I upstream and downstream cofferdams at Tobacco spillway.
- 6. Demolish Tobacco spillway.
- 7. Construct new auxiliary labyrinth spillway and gated spillway at Tobacco Dam.
- 8. Reconstruct Tobacco Dam flanking embankments from M-30 causeway to right abutment.
- 9. Restore Tobacco River channel.
- 10. Remove Phase I cofferdams and construct Phase II cofferdams at Edenville Spillway and Powerhouse.
- 11. **Divert water from Tittabawassee River through M-30 Diversion through Tobacco spillway into the Tobacco River Channel.**
- 12. Demolish Edenville spillway and powerhouse.
- 13. Construct new auxiliary spillway and gated spillway at Edenville Dam.
- 14. Reconstruct Edenville Dam flanking embankment from M-30 causeway to left abutment.
- 15. Restore Tittabawassee River channel.
- 16. Remove Phase II cofferdams.
- 17. Remove M-30 causeway control structure and restore M-30 bridge.
- 18. Refill Wixom Lake and, monitor performance.
- 19. Final site restoration and contractor demobilizations.

Special Consideration

• The County Highway M-30 bridge and causeway embankment that separates Wixom Lake at the Edenville Dam project failed during the May 2020 storm. Since the failure, the Tobacco River flow is conveyed to the Tittabawassee River through the M-30 and Edenville Dam breach channels. We understand the Michigan Department of Transportation is currently

working on plans to rebuild the M-30 bridge to restore the corridor across Wixom Lake. During construction, a temporary control structure will likely be needed at the M-30 corridor to divert a portion of the Tobacco and Tittabawassee River flows through either the Tobacco or Edenville gated spillways (see Figure 11).

Smallwood Dam

- 1. Fully draw down impoundment, stabilize existing project structures, remove debris and inspect spillway and powerhouse. (To be completed by Boyce).
- 2. Contractor mobilization, left and right abutment reconstruction and develop laydown and contractor work areas.
- 3. Rehabilitate the left and right embankments and install downstream erosion protection.
- 4. Construct new auxiliary labyrinth spillway at left abutment and armor discharge channel.
- 5. Repair and stabilize the gated spillway, tailrace area and replace gate hoists and actuators as needed.
- 6. Decommission and remove the turbine-generator set. Convert water passage to gated low-level outlet and backfill with cellular concrete and stabilize structure.
- 7. Refill Smallwood Lake and monitor performance.
- 8. Final site restoration and contractor demobilizations.

Secord Dam

- 1. Fully draw down impoundment, stabilize existing project structures, remove debris and inspect spillway and powerhouse. (To be completed by Boyce).
- 2. Contractor mobilization, left and right abutment reconstruction and develop laydown and contractor work areas.
- 3. Decommission and remove Tainter gates. Convert water passage to gated low level outlet, backfill with cellular concrete and underpin structure.
- 4. Construct new auxiliary labyrinth spillway and increase flow capacity by cutting down the ogee crest, underpinning, backfilling with cellular concrete and installing larger crest gates. Modify training walls and stilling basin as needed.
- 5. Rehabilitate and stabilize left and right embankments.
- 6. Refill Secord Lake and monitor performance.
- 7. Final site restoration and contractor demobilizations.

The exact sequence of construction by dam could vary from the sequence presented above, for example, rehabilitate Secord and Smallwood prior to reconstruction of Edenville and Sanford Dams. However, in general, Sanford should be reconstructed prior to and ready to receive flows prior to reconstruction of Edenville Dam to mitigate the potential for damage at and downstream of Sanford Dam due to possible increased flow releases from Edenville Dam during or after construction.

Planning Level Cost Analysis

Opinions of probable construction cost (OPCC) were developed for the four project configurations to pass the ½ PMF based on the proposed project facilities and construction approaches presented in this report. The level of detail for this type of estimate is assumed to provide construction cost within the range of -30 to +50%, typically used for conceptual design studies. The OPCC includes 30% contingency for all construction items and includes an allowance of 8% to 15% of the total construction cost for site investigations, engineering design, permitting and construction engineering / management costs. The range of OPPC was approximately \$14 million for the Secord Dam up to approximately \$208 million for the Edenville Dam repairs. The total OPCC for each of the four dams to pass the ½ PMF was approximately \$337 million. A summary of the ½ PMF OPPC for each of the four projects is summarized in **Table 7** through **Table 10** with the total project costs provided in **Table 11.** ½ PMF OPCC estimate worksheets are provided as **Attachment 3**.

The FLTF have also requested that GEI develop an OPCC to pass the full PMF in case the State of Michigan EGLE increases the required high hazard dam minimum spillway capacity requirement above the ½ PMF or if, at a future date, the probable maximum precipitation estimates for the region increase. The project configurations described in the sections above were expanded to include additional spillway capacity to accommodate the full PMF by providing additional primary spillway gates, longer auxiliary labyrinth spillways, and expanded upstream and downstream cellular cofferdams. For the purposes of this analysis, the primary gated spillway was sized to pass approximately 75% of the PMF, and the remaining 25% of the PMF was passed through the auxiliary labyrinth spillways. During preliminary design, this ratio will be optimized to an appropriate recurrence interval storm to be passed through the primary gated spillway, and the remainder above the selected the recurrence interval will be passed through the auxiliary labyrinth spillways. For example, the primary gated spillways could be sized to pass the 500- to 1,000-year storm event and the auxiliary spillway will be sized to pass the remaining flow up to the PMF. Without these recurrence interval statistics available at this time, the assumed gated to passive spillway ratio of 75% / 25% is considered appropriate for this level of OPCC.

A summary of the PMF OPCC for each of the four projects is summarized in **Table 7** through **Table 10** with the total project costs provided in **Table 11**. A bulleted summary precedes each project table highlighting the major additional construction activities needed to increase spillway capacity from the ½ PMF to the full PMF. PMF OPCC estimate worksheets are provided as **Attachment 4**.

Sanford Dam - Additional Construction Activities to Increase Spillway Capacity to the PMF

- Increase the size and footprint of the cellular cofferdam for the demolition of the existing powerhouse and primary gated spillway and the construction of a new wider primary gated spillway.
- Increase the number of 22-foot wide crest gates on the primary spillway from six (6) to twelve (12).
- Increase the footprint of the cellular cofferdam for the construction of a wider auxiliary labyrinth spillway on the right embankment.
- Increase the width of the auxiliary labyrinth spillway from 165-foot wide to 250-foot wide.
- Reduce the amount of right embankment reconstruction due to the increased width of the primary gated spillway and auxiliary labyrinth spillway.

Table 7: Summary of Opinion of Probable Construction Costs – Sanford Dam

Item	Description	½ PMF	F	ull PMF
0.00	General Conditions	\$ 5,297,000	\$	7,356,000
1.00	Site Preparation and Cofferdams	\$ 14,260,000	\$	21,775,000
2.00	Demolition / Abandonment	\$ 5,250,000	\$	5,250,000
3.00	Left Abutment Reconstruction	\$ 1,119,000	\$	1,110,000
4.00	Right Embankment Reconstruction	\$ 16,421,000	\$	13,130,000
5.00	New Gated Spillway / Outlet Works	\$ 15,326,000	\$	30,700,000
6.00	New Labyrinth Spillway Structure	\$ 5,677,000	\$	8,960,000
7.00	Site Restoration	\$ 250,000	\$	250,000
	Subtotal	\$ 63,600,000	\$	88,531,000
	30% Contingency	\$ 19,080,000	\$	26,559,000
	Construction Subtotal	\$ 82,680,000	\$	115,090,000
	Site Investigations, Engineering, Permitting and			
	Construction Management (10%)	\$ 8,268,000	\$	11,509,000
	Total Estimated Cost	\$ 90,948,000	\$	126,599,000

Edenville Dam - Additional Construction Activities to Increase Spillway Capacity to the PMF

- Increase the size and footprint of the cellular cofferdam for the demolition of the existing powerhouse and primary gated spillways, and the construction of new wider primary gated spillways at Edenville and Tobacco. Increase the number of 24-foot wide crest gates on the Edenville and Tobacco primary spillways from three (3) to six (6).
- Increase the width of the Edenville and Tobacco auxiliary labyrinth spillways from 125-foot wide to 200-foot wide.
- Reduce the amount of embankment reconstruction due to the increased width of the primary gated spillways and auxiliary labyrinth spillways.

Table 8: Summary of Opinion of Probable Construction Costs – Edenville Dam

Item	Description	1	/ ₂ PMF	I	Full PMF
0.00	General Conditions	\$	12,258,000	\$	14,678,000
1.00	Site Preparation and Cofferdams	\$	31,620,000	\$	39,730,000
2.00	M-30 Diversion	\$	4,000,000	\$	4,000,000
3.00	Demolition / Abandonment	\$	5,750,000	\$	5,750,000
4.00	Edenville Embankments - Breached Section	\$	13,406,000	\$	13,406,000
5.00	Edenville Embankments - Repaired and Stabilized	\$	31,370,000	\$	29,159,000
6.00	Tobacco Embankments - Repaired and Stabilized	\$	22,186,000	\$	20,360,000
7.00	New Gated Spillways and Outlet Works - Edenville	\$	7,865,000	\$	15,730,000
8.00	New Gated Spillways and Outlet Works - Tobacco	\$	7,865,000	\$	15,730,000
9.00	New Labyrinth Spillway Structure - Edenville	\$	5,542,000	\$	9,085,000
10.00	New Labyrinth Spillway Structure - Tobacco	\$	5,542,000	\$	9,085,000
11.00	Site Restoration	\$	500,000	\$	500,000
	Subtotal	\$	147,904,000	\$	177,213,000
	30% Contingency	\$	44,371,000	\$	53,164,000
	Construction Subtotal	\$	192,275,000	\$	230,377,000
	Site Investigations, Engineering, Permitting and Construction Management (8%)	\$	15,382,000	\$	18,430,000
	Total Estimated Cost	\$	207,657,000	\$	248,807,000

Smallwood Dam – Additional Construction Activities to Increase Spillway Capacity to the PMF

- Construct cellular cofferdam upstream and downstream of the existing powerhouse and gated spillway. Demolish the existing primary gated spillway and powerhouse.
- Construct new wider primary gated spillway with five (5) new 24-foot wide crest gates.
- Increase the width of the auxiliary labyrinth spillway from 125-foot wide to 180-foot wide.
- Reduce the amount of embankment rehabilitation due to the increased width of the primary gated spillways and auxiliary labyrinth spillways.

Table 9: Summary of Opinion of Probable Construction Costs – Smallwood Dam

Item	Description	½ PMF		Full PMF
0.00	General Conditions	\$	802,000	\$ 2,704,000
1.00	Site Preparation and Cofferdams	\$	270,000	\$ 7,137,000

2.00	Powerhouse Demolition	\$ 500,000	\$ 4,250,000
3.00	Left Embankment Repair and Stabilization	\$ 794,000	\$ 794,000
4.00	Right Embankment Repair and Stabilization	\$ 371,000	\$ 252,000
5.00	Gated Spillways	\$ 1,880,000	\$12,077,000
6.00	Powerhouse Rehabilitation	\$ 960,000	\$ -
7.00	Auxiliary Spillway Structure	\$ 3,446,000	\$ 4,846,000
8.00	Site Restoration	\$ 130,000	\$ 130,000
	Subtotal	\$ 9,153,000	\$32,190,000
	30% Contingency	\$ 2,746,000	\$ 9,657,000
	Construction Subtotal	\$ 11,899,000	\$41,847,000
	Site Investigations, Engineering, Permitting and		
	Construction Management (15%)	\$ 1,785,000	\$ 6,277,000
	Total Estimated Cost	\$ 13,684,000	\$48,124,000

Secord Dam – Additional Construction Activities to Increase Spillway Capacity to the PMF

- Construct cellular cofferdam upstream and downstream of the existing powerhouse and gated spillway.
- Demolish the existing primary gated spillway and powerhouse.
- Construct new primary gated spillway with four (4) new 24-foot wide crest gates.
- Replace the 200-foot wide passive overflow weir structure with a new 200-foot wide auxiliary labyrinth spillway.

Table 10: Summary of Opinion of Probable Construction Costs – Secord Dam

Item	Description	½ PMF	Full PMF
0.00	General Conditions	\$ 1,392,000	\$ 3,088,000
1.00	Site Preparation and Cofferdams	\$ 220,000	\$ 7,087,000
2.00	Powerhouse Decommissioning and TG Abandonment	\$ 500,000	\$ 4,250,000
3.00	Left Embankment Repair and Stabilization	\$ 3,341,000	\$ 3,341,000
4.00	Right Embankment Repair and Stabilization	\$ 2,555,000	\$ 2,552,000
5.00	Gated Spillway Rehabilitation	\$ 3,298,000	\$10,887,000
6.00	Powerhouse Rehabilitation	\$ 1,946,000	\$ -
7.00	Auxiliary Spillway Structure	\$ 2,928,000	\$ 5,512,000
8.00	Site Restoration	\$ 130,000	\$ 130,000
Subtotal		\$16,310,000	\$36,847,000
Contingency		\$ 4,893,000	\$11,054,000
Construction Subtotal		\$21,203,000	\$47,901,000
Site Investigations, Engineering, Permitting and Construction Management (15%)		\$ 3,180,000	\$ 7,185,000
Total Estimated Cost		\$24,383,000	\$55,086,000

The incremental cost needed to increase spillway capacity from the ½ PMF to the PMF is approximately 42% higher or \$141,944,000. We consider the range of costs presented appropriate for the intended use of the County's assessors to estimate the current value of assets and liabilities associated with acquiring these from Boyce. The project configurations described in this TM will be further refined and optimized during the preliminary design phase to economically pass the selected design storm (1/2 PMF or Full PMF) safely.

Full PMF Dam 1/2 PMF \$ 90,948,000 \$ 126,599,000 Sanford Dam \$ Edenville Dam \$ 207,657,000 248,807,000 48,124,000 \$ \$ Smallwood Dam 13,684,000 Secord Dam \$ \$ 55,086,000 24,383,000 **Total** \$ 336,672,000 \$ 478,616,000

Table 11: Summary of Opinion of Probable Construction Costs

Closing

Our opinions of probable cost should be considered rough budgetary estimates based on conceptual level designs, costs for similar projects and engineering judgment. Detailed designs and quantities have not yet been prepared. Actual bids and total project costs may vary based on contractor's perceived risk, site access, season, market conditions, etc. No warranties concerning the accuracy of costs presented herein are expressed or implied.

Enclosed

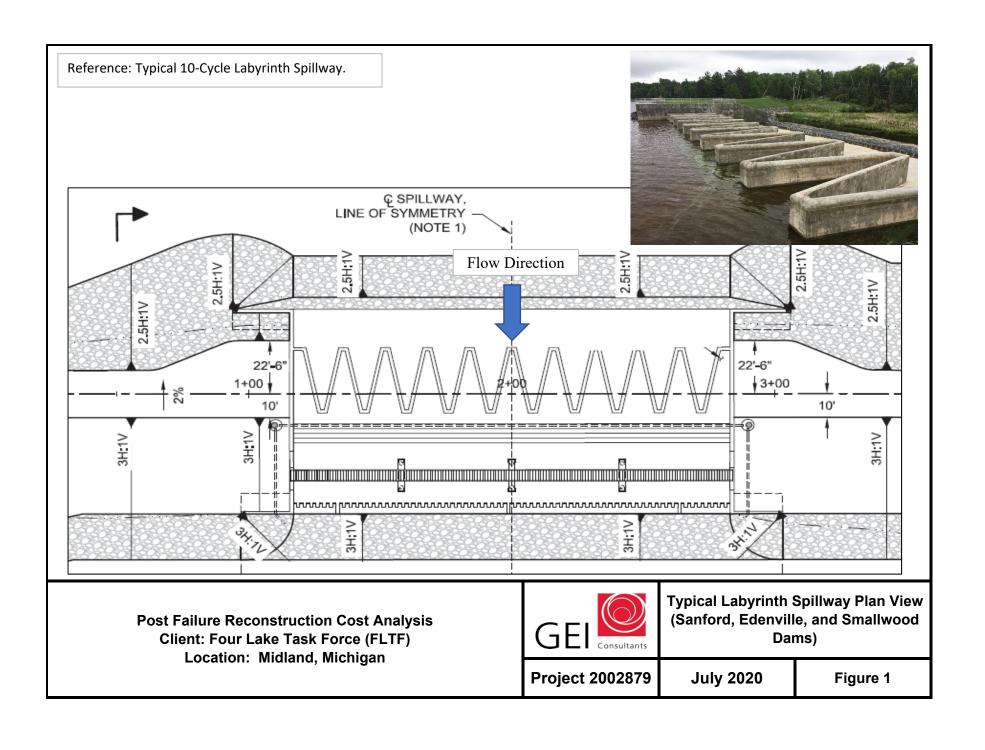
- Figure 1 Typical Labyrinth Spillway Plan View (Sanford, Edenville and Smallwood Dams)
- Figure 2 Typical Embankment Reconstruction Cross Section (Sanford and Edenville Dams)
- Figure 3 Smallwood Dam Auxiliary Spillway Isometric View
- Figure 4 Smallwood Dam Embankment Rehabilitation Cross Section View
- Figure 5 Secord Dam Auxiliary Spillway Plan View
- Figure 6 Secord Dam Embankment Rehabilitation Cross Section View
- Figure 7 Sanford Dam Gated Spillway Cofferdam Plan
- Figure 8 Sanford Dam Auxiliary Spillway and Breach Channel Cofferdam Plan
- Figure 9 Edenville Dam Tobacco Spillway Cofferdam Plan
- Figure 10 Edenville Dam Edenville Spillway and Breach Channel Cofferdam Plan
- Figure 11 M-30 Control Structure Location Plan

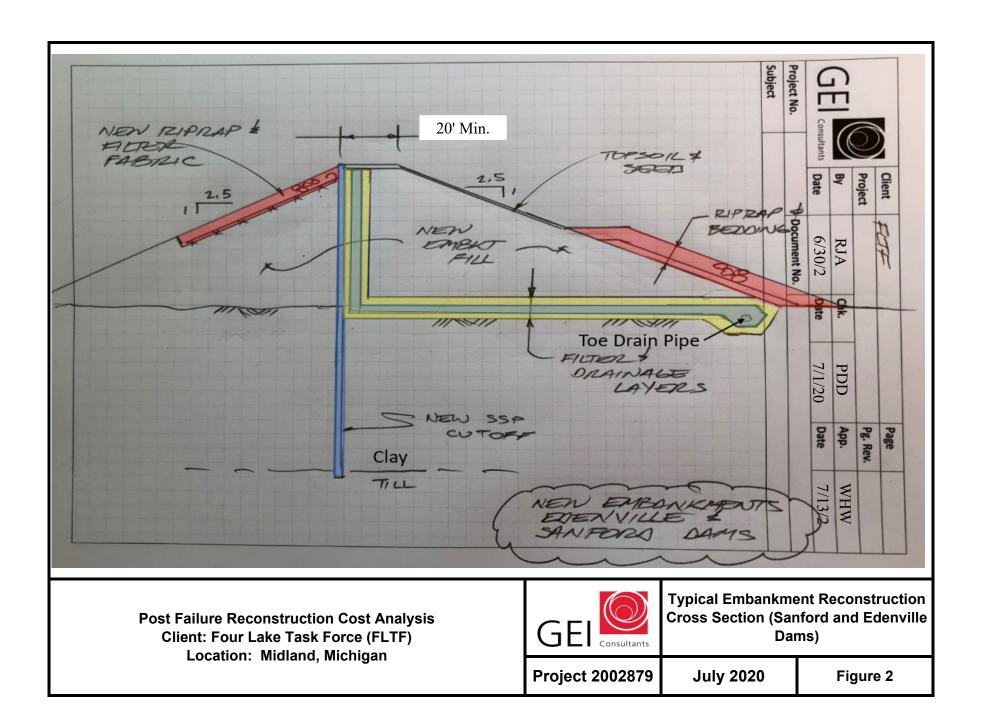
Attachment 1 – Pre and Post Failure Project Photographs

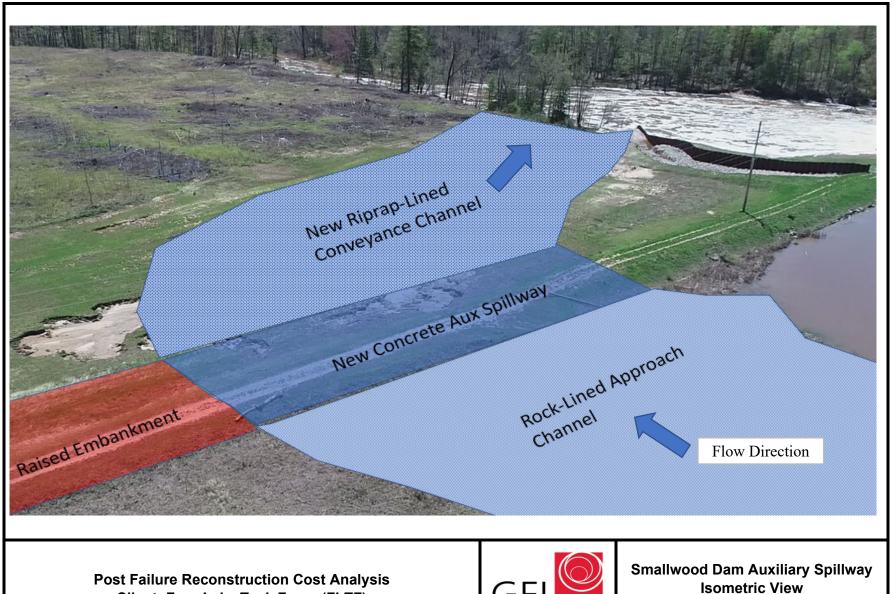
Attachment 2 – Concept Level Spillway Rating Curves

Attachment 3 – OPCC Estimate Worksheets – ½ PMF

Attachment 4 – OPCC Estimate Worksheets – PMF





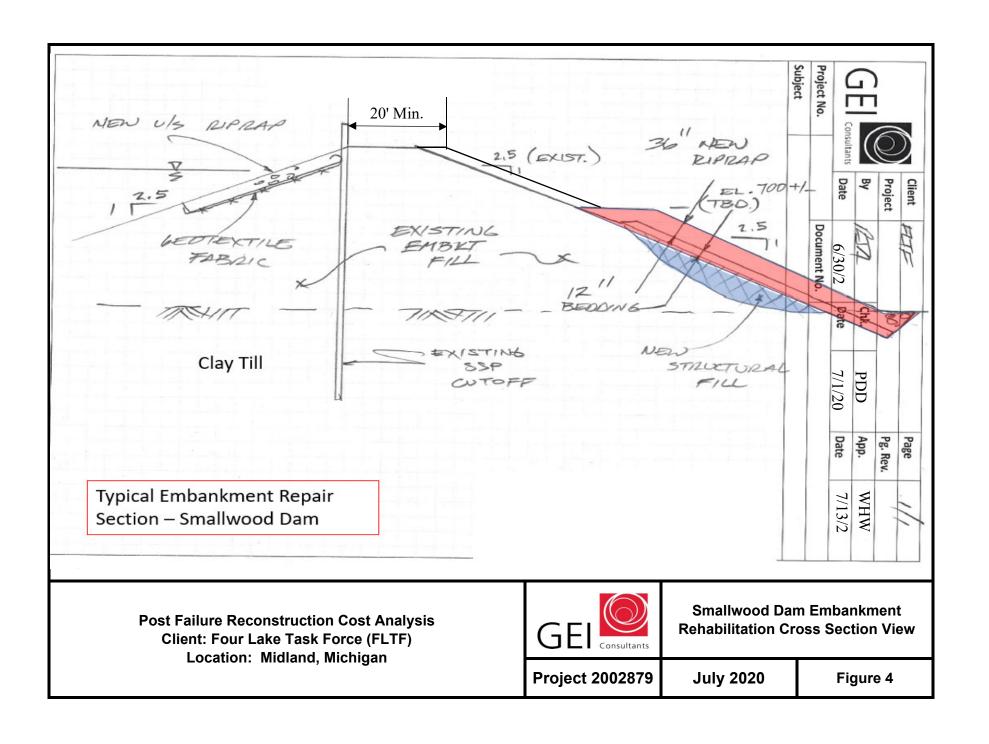


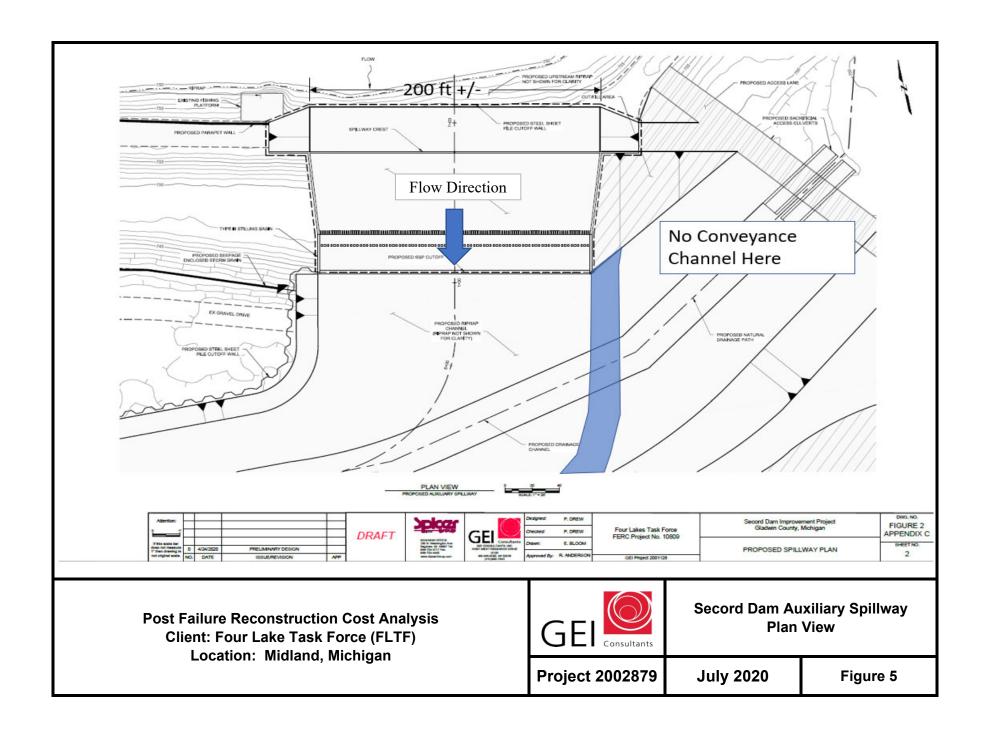
Client: Four Lake Task Force (FLTF) Location: Midland, Michigan

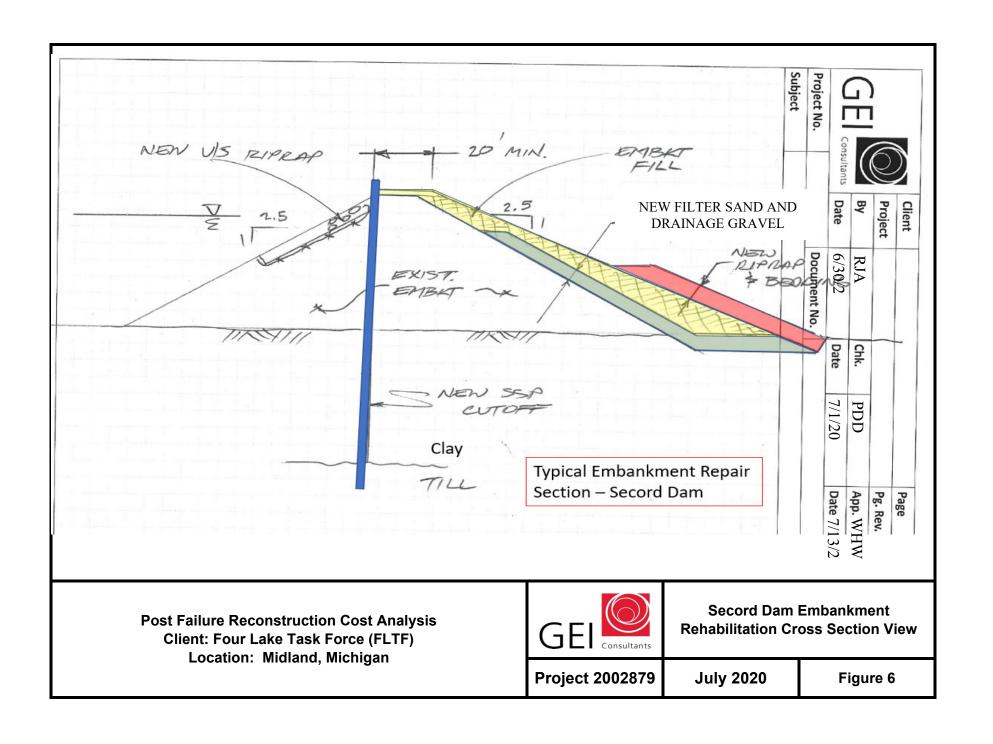


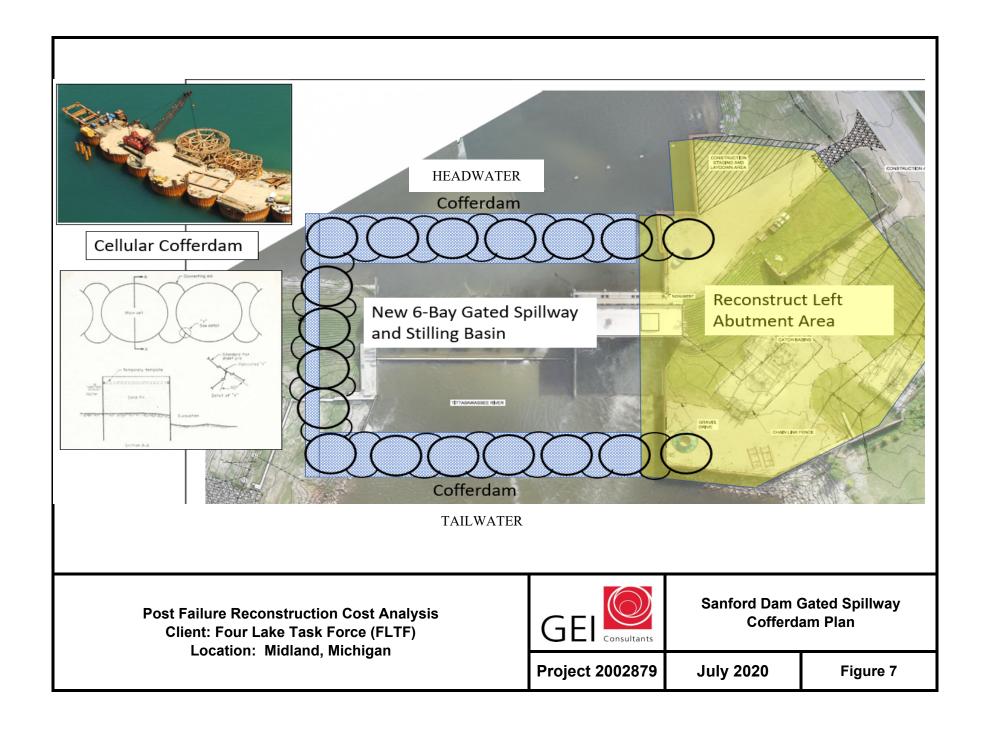
Project 2002879

July 2020

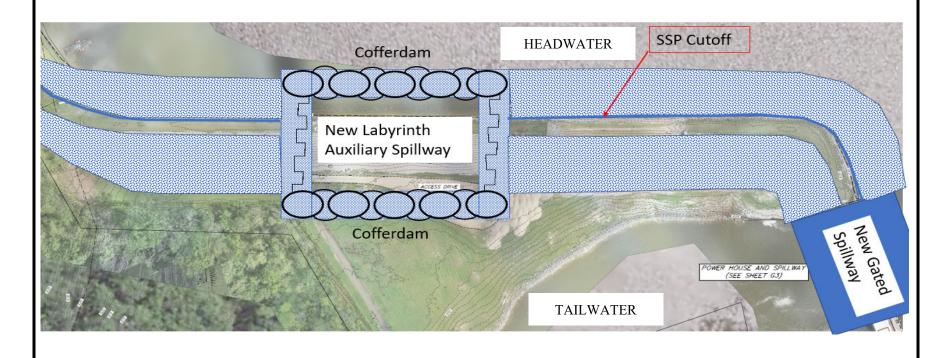








Breach Area Cofferdam and Right Embankment Access



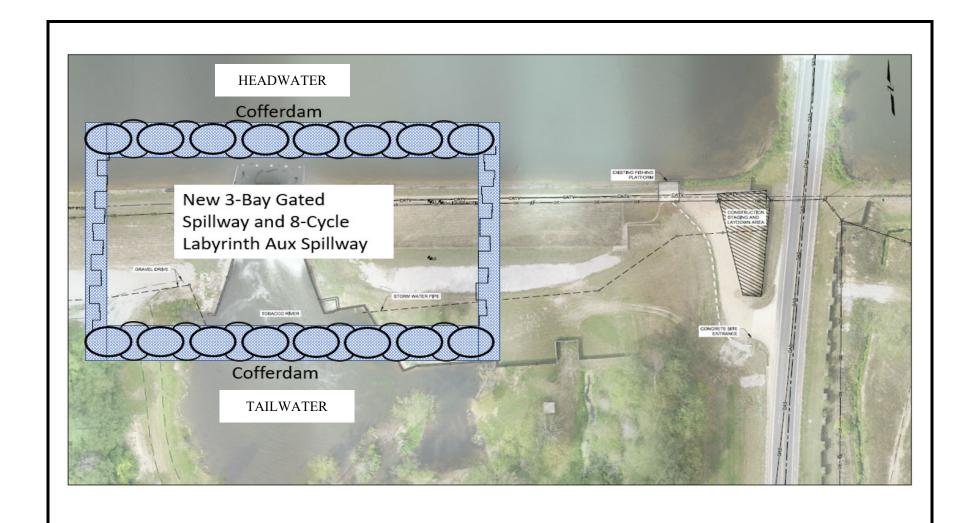
Post Failure Reconstruction Cost Analysis Client: Four Lake Task Force (FLTF) Location: Midland, Michigan



Sanford Dam Auxiliary Spillway and Breach Channel Cofferdam Plan

Project 2002879

July 2020



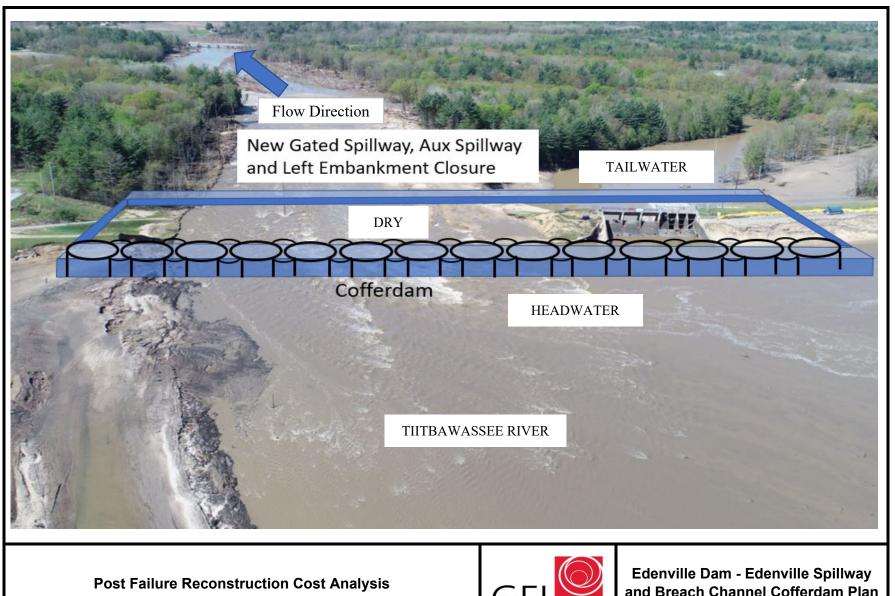
Post Failure Reconstruction Cost Analysis
Client: Four Lake Task Force (FLTF)
Location: Midland, Michigan



Edenville Dam - Tobacco Spillway
Cofferdam Plan

Project 2002879

July 2020

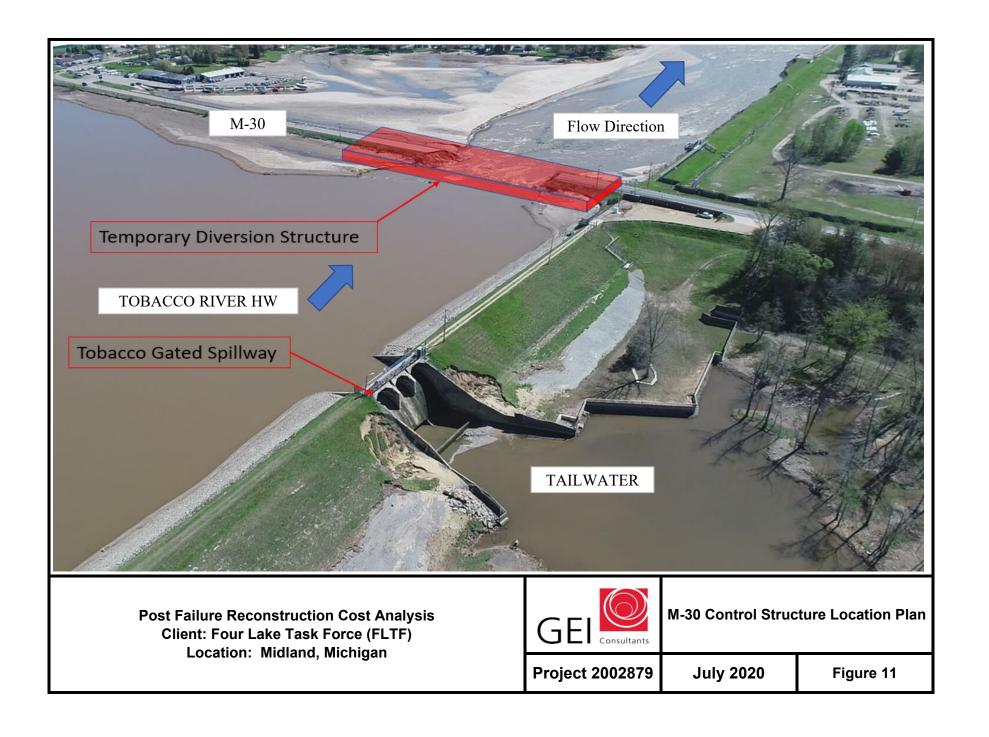


Client: Four Lake Task Force (FLTF) Location: Midland, Michigan

and Breach Channel Cofferdam Plan

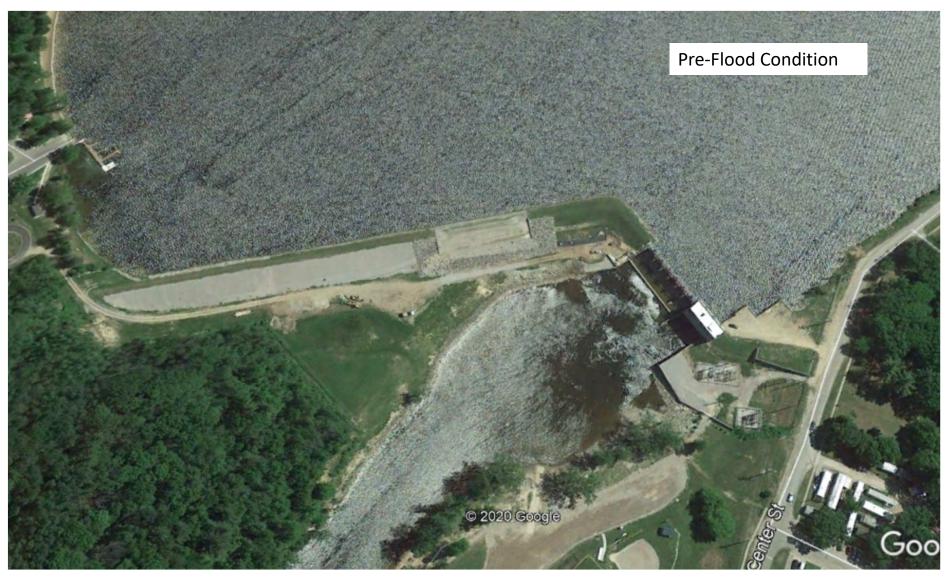
Project 2002879

July 2020

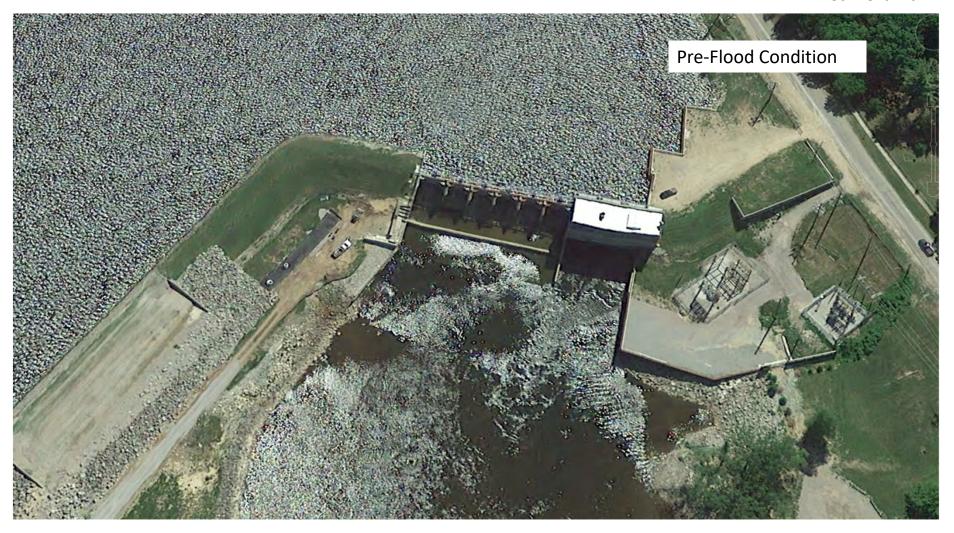


Attachment 1 – Pre and Post Failure Project Photographs

Sanford Dam



Sanford Dam



Sanford Dam



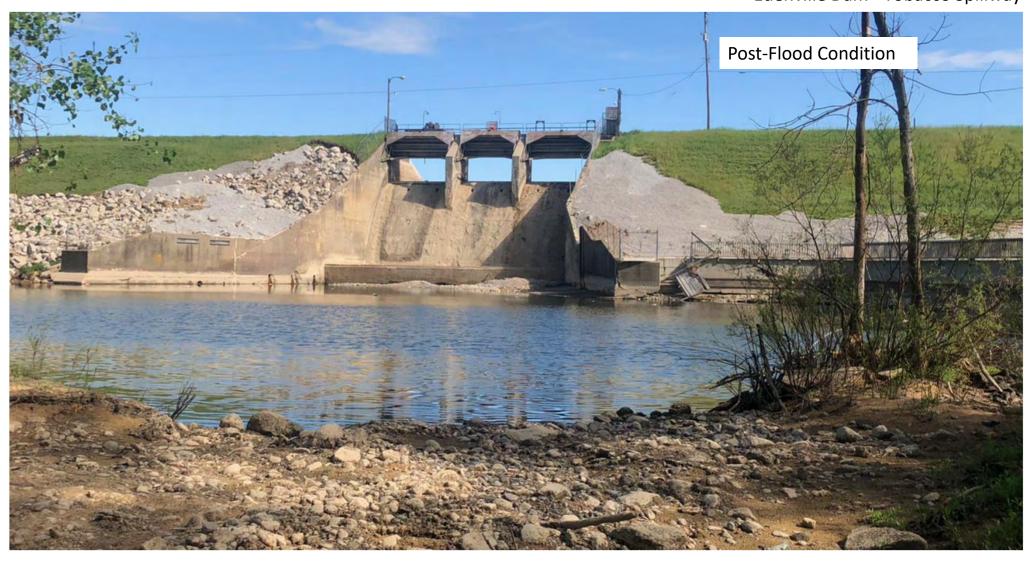
Edenville Dam - Tobacco Spillway



Edenville Dam - Tobacco Spillway



Edenville Dam - Tobacco Spillway



Edenville Dam - Tobacco Spillway



Edenville Dam - Edenville Spillway



Edenville Dam - Edenville Spillway



Edenville Dam - Edenville Spillway













Attachment 2 – Concept Level Spillway Rating Curves



Client:	Four Lakes Task Force	Project #:	2002879	Page:	
Project:	Sanford Dam	By:	PDD	Date:	6/19/2020
Subject:	Rating Curve Calculations	Checked:	RJA	Date:	7/13/2020
		Approved:	WHW	Date:	7/13/2020

Ogee Spillway Discharge Rating Curve - Tainter Gates (Fully Open)

Input Parameter	Gate#1	Gate #2	Gate #3	Gate #4	Gate #5	Gate #6	Unit
Crest Length	22	22	22	22	22	22	feet
Crest El.	620	620	620	620	620	620	NGVD29 feet
Ogee Design Head (Ho)	11	11	11	11	11	11	feet
Approach El.	600.3	600.3	600.3	600.3	600.3	600.3	
Approach Depth (P)	19.7	19.7	19.7	19.7	19.7	19.7	feet
Number of Piers	1	2	2	2	2	1	-
Abutment coeff (Ka)	0.1	0	0	0	0	0.1	-
Pier coeff (Kp)	0	0	0	0	0	0	
Top of Non-Overflow El.	635.6	636.8	636.8	636.8	636.8	636.8	feet
P/Ho	1.79	1.79	1.79	1.79	1.79	1.79	
Design Head Coeff.	3.92	3.92	3.92	3.92	3.92	3.92	Figure 9-23
							-

Reference: STID

STID

from Upper Nappe Profile Tab

Discharge, Q = Leff*C*H^{3/2}

L=L'- 2 (NKP +Ka) He

USBR DOSD 1987

								Wei	r Flow								
Reservoir El.	Total Head, He	He / Ho	Ratio of Coeff. c/co	Adjusted Coeff., c	Eff. Length (Gate 1)	Eff. Length (Gate 2)	Eff. Length (Gate 3)	Eff. Length (Gate 4)	Eff. Length (Gate 5)	Eff. Length (Gate 6)	Discharge (Gate 1)	Discharge (Gate 2)	Discharge (Gate 3)	Discharge (Gate 4)	Discharge (Gate 5)	Discharge (Gate 6)	Discharge (All Gates)
ft	ft	-	-	-	ft	ft	ft	ft	ft	ft	cfs						
620.0	0.0	0.0	0.78	3.06	22.0	22.0	22.0	22.0	22.0	22.0	0	0	0	0	0	0	C
622.5	2.5	0.2	0.86	3.36	21.5	22.0	22.0	22.0	22.0		285	292	292	292	292	285	
623.0	3.0	0.3	0.87	3.40	21.4	22.0	22.0	22.0	22.0	21.4	379	389	389	389	389	379	
623.5	3.5	0.3	0.88	3.45	21.3	22.0	22.0	22.0				497	497	497	497	481	,
624.0	4.0	0.4	0.89	3.49	21.2	22.0	22.0	22.0	22.0	21.2		615	615	615		592	
624.5	4.5	0.4	0.90	3.53	21.1	22.0	22.0	22.0	22.0			742	742	742		711	,
625.0	5.0	0.5	0.91	3.57	21.0	22.0	22.0		22.0		838	878	878	878	878	838	-,
625.5	5.5	0.5	0.92	3.61	20.9	22.0	22.0					1,023	1,023	1,023	1,023	972	
626.0	6.0	0.5	0.93	3.64	20.8	22.0	22.0				, -	1,177	1,177	1,177	1,177	1,113	
626.5	6.5	0.6	0.94	3.67	20.7	22.0	22.0				,	1,339	1,339	1,339	,	1,260	,
627.0	7.0	0.6	0.95	3.70	20.6	22.0	22.0				,	1,509	1,509	1,509	1,509	1,413	
627.5	7.5	0.7	0.95	3.73	20.5	22.0	22.0					1,687	1,687	1,687	1,687	1,572	-,
628.0	8.0	0.7	0.96	3.76	20.4	22.0	22.0		22.0		, -	1,874	1,874	1,874	1,874	1,737	-,
628.5	8.5	0.8	0.97	3.79	20.3	22.0	22.0					2,067	2,067	2,067	2,067	1,908	
629.0	9.0	0.8	0.98	3.82	20.2	22.0					,	2,269	2,269	2,269	2,269	2,083	
629.5	9.5	0.9	0.98	3.85	20.1	22.0	22.0		22.0		,	2,477	2,477	2,477	2,477	2,263	,
630.0	10.0	0.9	0.99	3.87	20.0	22.0	22.0					2,694	2,694	2,694	2,694	2,449	
630.5	10.5	1.0	1.00	3.90	19.9	22.0	22.0					2,917	2,917	2,917	2,917	2,639	
631.0	11.0	1.0	1.00	3.92	19.8	22.0	22.0				,	3,148	3,148	3,148		2,833	
631.5	11.5	1.0	1.01	3.95	19.7	22.0	22.0					3,386	3,386	3,386	3,386	3,032	-,
632.0	12.0	1.1	1.01	3.97	19.6	22.0	22.0		22.0		,	3,630	3,630	3,630	3,630	3,234	
632.5	12.5	1.1	1.02	3.99	19.5	22.0	22.0		22.0			3,882	3,882	3,882	3,882	3,441	
633.0	13.0	1.2	1.03	4.02	19.4	22.0	22.0				-,	4,140	4,140	4,140	,	3,651	
633.5	13.5	1.2	1.03	4.04	19.3	22.0	22.0					4,406	4,406	4,406	,	3,865	
634.0	14.0	1.3	1.04	4.06	19.2	22.0	22.0		22.0			4,677	4,677	4,677	4,677	4,082	
634.5	14.5	1.3	1.04	4.08	19.1	22.0	22.0		22.0		,	4,954	4,954	4,954	4,954	4,301	
634.8	14.8	1.3	1.04	4.09	19.0	22.0	22.0	22.0				5,124	5,124	5,124	,	4,434	
635.0	15.0	1.4	1.05	4.10	19.0	22.0	22.0					5,238	5,238	5,238		4,524	
635.5	15.5	1.4	1.05	4.12	18.9	22.0	22.0				, -	5,527	5,527	5,527	5,527	4,748	- ,
636.0	16.0	1.5	1.06	4.13	18.8	22.0	22.0	22.0	22.0	18.8	4,975	5,821	5,821	5,821	5,821	4,975	33,234

LABYRINTH WEIR DESIGN No Approach Velocity

 PROJECT:
 Sanford Labyrinth
 TIME:
 14:12:19

 PROJECT NO.
 2002879
 DATE:
 13-Jul-20

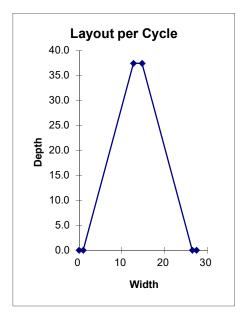
 FLOOD CRITERIA:
 1/2 PMF
 BY:
 PDD

	USER INPUT								
Max. Res	Zr	636.0 ft	Thickness						
Crest el.	Zc	632.5 ft	Wall	Tw	1.25 ft				
Floor el.	Zf	628.0 ft	Slab	Ts	1.25 ft				
Spillway width	Ws	165.0 ft	Cutoff Depth						
Apex Width	2a	2 ft	Sheet Pile	Ds	1 ft				
No. of cycles	n	6	Conc Wall	Dc	1 ft				
Magnification	L/W	3							

Note: L_{de}/B must be <= 0.35 Ho/P must be <= 0.9 α must be >= 6 deg

CRES1	LAYOUT	
	(One Cycle)	

X Y
0 0 0
1.00 0
12.75 37.45
14.75 37.45
26.50 0
27.50 0



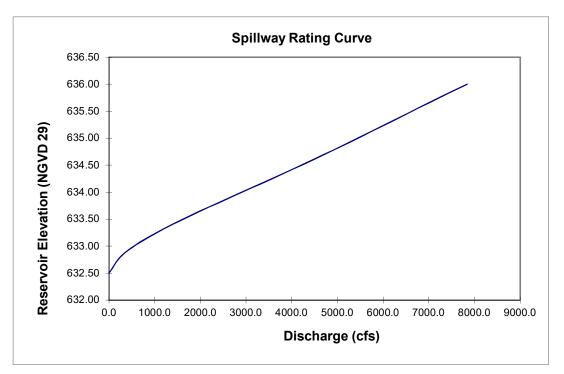
LABYRINTH DIMENSIONS (Per Cycle) Wall Height 4.5 **ft** Ρ Width W 27.50 ft Length L 82.50 ft Wall Length В 39.25 ft Depth D 37.45 **ft** Head max Н 3.50 ft Wall Angle α 17.42 deg Length of L_{de} 8.66 ft Interference

Qmax 7,837 cfs

COEFFICIENTS	_
Column	4.00
Cd lower	0.40
Cd Upper	0.46
Cd	0.45
Efficacy	1.80

RATING CURVE

HEAD	H _o /P	C_{lower}	C_{upper}	C _d	Q	RES
3.50	0.78	0.40	0.46	0.45	7837	636.00 1/2 PMF EI.
3.15	0.70	0.42	0.48	0.47	6987	635.65
2.80	0.62	0.44	0.51	0.50	6157	635.30
2.45	0.54	0.47	0.54	0.52	5324	634.95
2.10	0.47	0.50	0.57	0.55	4464	634.60
1.75	0.39	0.53	0.59	0.58	3567	634.25
1.40	0.31	0.56	0.61	0.60	2648	633.90
1.05	0.23	0.57	0.62	0.61	1747	633.55
0.70	0.16	0.57	0.61	0.60	936	633.20
0.35	0.08	0.55	0.57	0.57	310	632.85
0.00	0.00	0.49	0.49	0.49	0	632.50



Discharge Coefficient Table Tullis et al. (1995)

		Angle wall makes with centerline α									
	6	8	12	15	18	25	35	90			
A0	0.49	0.49	0.49	0.49	0.49	0.49	0.49	0.49			
A1	-0.24	1.08	1.06	1.00	1.32	1.51	1.69	1.46			
A2	-1.20	-5.27	-4.43	-3.57	-4.13	-3.83	-4.05	-2.56			
A3	2.17	6.79	5.18	3.82	4.24	3.40	3.62	1.44			
A4	-1.03	-2.83	-1.97	-1.38	-1.50	-1.05	-1.10				



Client:	Four Lakes Task Force	Project #:	2002879	Page:	
Project:	Edenville Dam	By:	PDD	Date:	6/19/2020
Subject:	Rating Curve Calculations	Checked:	RJA	Date:	7/13/2020
		Annroyed:	\\/H\\/	Date:	7/13/2020

Ogee Spillway Discharge Rating Curve - Tainter Gates (Fully Open) Edenville Tobacco Input Parameter Gate#1 Gate #2 Gate #3 Gate #1 Gate #2 Gate #3 Unit Crest Length 24 feet 24 24 24 24 Crest El. 665.5 665.5 NGVD29 feet 665.5 665.5 665.5 665.5 Ogee Design Head (Ho) 12 12 12 12 12 12 feet Approach El. 628.3 628.3 628.3 628.3 628.3 628.3 Approach Depth (P) 37.2 37.2 37.2 37.2 37.2 37.2 feet Number of Piers Abutment coeff (Ka) 0.15 0.15 0.15 0.15 0 Pier coeff (Kp) 0.01 0.01 0.01 0.01 0.01 0.01 Top of Non-Overflow El. 636.8 636.8 636.8 636.8 636.8 636.8 feet 3.10 3.10 3.10 P/Ho 3.10 3.10 3.10 Design Head Coeff. 3.93 3.93 3.93 3.93 3.93 3.93 Figure 9-23 Max Opening Height

Reference: STID STID

from Upper Nappe Profile Tab

Discharge, $Q = Leff*C*H^{3/2}$

L=L'- 2 (NKP +Ka) He

USBR DOSD 1987 From Gate Test Notes

								1	Weir Flow									
Reservoir El.	Total Head, He	He / Ho	Ratio of Coeff. c/co	Adjusted Coeff., c	Eff. Length (Edenville Gate 1)	Eff. Length (Edenville Gate 2)	Eff. Length (Edenville Gate 3)	Eff. Length (Tobacco Gate 1)	Eff. Length (Tobacco Gate 2)	Eff. Length (Tobacco Gate 3)	Discharge (Edenville Gate 1)	Discharge (Edenville Gate 2)	Discharge (Edenville Gate 3)	Discharge (Tobacco Gate 1)	Discharge (Tobacco Gate 2)	Discharge (Tobacco Gate 3)	Edenville Gates	Tobacco Gates
ft	ft	-	-	-	ft	ft	ft	ft	ft	ft	cfs	cfs	cfs	cfs	cfs	cfs	cfs	cfs
665.5	0.0	0.0		3.08			24.0		24.0	24.0		0	0	0	0	0	0	0
668.0	2.5	0.2		3.35			23.2		23.9	23.2		316	307	307		307	930	
668.5	3.0	0.3		3.39			23.0	23.0	23.9	23.0		421	406	406	421	406	1,234	
669.0	3.5	0.3		3.44			22.9	22.9	23.9	22.9		537	515	515	537	515	1,566	
669.5	4.0	0.3		3.48			22.7	22.7	23.8	22.7	632	663	632	632	663	632	1,927	,-
670.0	4.5	0.4	0.89	3.51			22.6	22.6	23.8	22.6		799	757	757	799	757	2,313	
670.5	5.0	0.4	0.90	3.55			22.4	22.4	23.8	22.4		945	889	889	945	889	2,724	
671.0	5.5	0.5	0.91	3.59			22.2	22.2	23.8	22.2		1,100	1,029	1,029	1,100	1,029	3,157	
671.5	6.0	0.5	0.92	3.62		23.8	22.1	22.1	23.8	22.1	1,174	1,264	1,174	1,174	1,264	1,174	3,612	
672.0	6.5	0.5	0.93	3.65			21.9	21.9	23.7	21.9	,	1,436	1,326	1,326	1,436	1,326	4,088	,
672.5	7.0	0.6		3.68			21.8	21.8	23.7	21.8		1,617	1,483	1,483	1,617	1,483	4,583	
673.0	7.5	0.6		3.71			21.6	21.6	23.7	21.6	,	1,806	1,646	1,646	1,806	1,646	5,097	5,097
673.5	8.0	0.7		3.74			21.4	21.4	23.7	21.4	1,813	2,003	1,813	1,813	2,003	1,813	5,629	
674.0	8.5	0.7	0.96	3.76			21.3	21.3	23.7	21.3	1,985	2,207	1,985	1,985	2,207	1,985	6,178	
674.5	9.0	0.8		3.79			21.1	21.1	23.6	21.1	2,162	2,420	2,162	2,162	2,420	2,162	6,744	
675.0	9.5	0.8		3.82			21.0	21.0	23.6	21.0	2,342	2,640	2,342	2,342	2,640	2,342	7,325	
675.5	10.0	0.8		3.84			20.8		23.6	20.8	,-	2,867	2,527	2,527	2,867	2,527	7,921	
676.0	10.5	0.9		3.87			20.6		23.6	20.6	, -	3,102	2,715	2,715	3,102	2,715	8,531	8,531
676.5	11.0	0.9	0.99	3.89			20.5	20.5	23.6	20.5	,	3,343	2,906	2,906	3,343	2,906	9,156	-,
677.0	11.5	1.0		3.91			20.3	20.3	23.5	20.3	-, -	3,592	3,101	3,101	3,592	3,101	9,794	
677.5	12.0 12.5	1.0		3.94 3.96			20.2	20.2	23.5	20.2		3,848	3,298	3,298	3,848	3,298	10,445	
678.0				3.96 3.98			20.0		23.5	20.0 19.8		4,111	3,498	3,498	4,111	3,498	11,108	
678.5	13.0 13.5	1.1		4.00			19.8	19.8 19.7	23.5 23.5	19.8		4,380 4,656	3,701	3,701 3,906	4,380	3,701	11,782	
679.0 679.5	13.5 14.0	1.1 1.2		4.00			19.7 19.5	19.7 19.5	23.5	19.7 19.5	3,906 4,113	4,656 4,939	3,906 4,113	3,906 4,113	4,656 4,939	3,906 4,113	12,468	12,468 13,164
680.0	14.0	1.2		4.02			19.5	19.5	23.4	19.5	4,113	5,227	4,113	4,113	5,227	4,113	13,164 13,870	
680.5	15.0	1.3		4.04			19.4		23.4	19.4		5,522	4,321	4,321	5,522	4,321		
	15.0			4.06		23.4	19.2	19.2	23.4	19.2	4,658	5,522	4,531	4,531 4,658	5,522	4,531	14,584	
680.8 681.0	15.3 15.5	1.3 1.3		4.07 4.08			19.1 19.0	19.1 19.0	23.4 23.4	19.1 19.0		5,702 5,823	4,658	4,658 4,742	5,702 5,823	4,658 4,742	15,017 15.307	
081.0	15.5	1.3	1.04	4.08	19.0	23.4	19.0	19.0	23.4	19.0	4,742	5,823	4,742	4,742	5,823	4,742	15,307	15,307

LABYRINTH WEIR DESIGN No Approach Velocity

 PROJECT:
 Edenville Labyrinth
 TIME:
 14:12:19

 PROJECT NO.
 2002879
 DATE:
 13-Jul-20

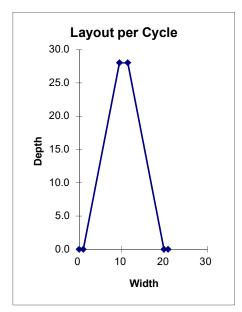
 FLOOD CRITERIA:
 1/2 PMF
 BY:
 PDD

USER INPUT								
Max. Res	Zr	681.0 ft	Thickness					
Crest el.	Zc	677.8 ft	Wall	Tw	1.25	ft		
Floor el.	Zf	673.0 ft	Slab	Ts	1.25	ft		
Spillway width	Ws	125.0 ft	Cutoff Depth					
Apex Width	2a	2 ft	Sheet Pile	Ds	1	ft		
No. of cycles	n	6	Conc Wall	Dc	1	ft		
Magnification	L/W	3						

Note: L_{de}/B must be <= 0.35 Ho/P must be <= 0.9 α must be >= 6 deg

CREST	Γ LAYOUT
	(One Cycle)

X	Υ
0	0
1.00	0
9.42	28.01
11.42	28.01
19.83	0
20.83	0



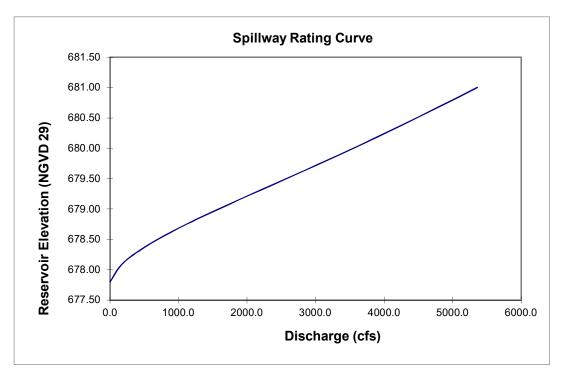
<u>LABYRINTH DIMENSIONS (Per Cycle)</u> Wall Height P 4.8 **ft** 20.83 ft Width W Length L 62.50 ft Wall Length В 29.25 ft Depth D 28.01 **ft** Head max Н 3.20 ft Wall Angle α 16.72 deg Length of L_{de} 8.21 ft Interference

DISCHARGE
Qmax 5,360 cfs

COEFFICIENTS	_
Column	4.00
Cd lower	0.43
Cd Upper	0.49
Cd	0.47
Efficacy	1.86

RATING CURVE

HEAD	H _o /P	\mathbf{C}_{lower}	C_{upper}	\mathbf{C}_{d}	Q	RES	
3.20	0.67	0.43	0.49	0.47	5360	681.00 1/2 PMF EI.	
2.88	0.60	0.45	0.52	0.49	4792	680.68	
2.56	0.53	0.48	0.54	0.51	4218	680.36	
2.24	0.47	0.50	0.57	0.54	3625	680.04	
1.92	0.40	0.53	0.59	0.56	3009	679.72	
1.60	0.33	0.55	0.61	0.58	2374	679.40	
1.28	0.27	0.57	0.62	0.60	1739	679.08	
0.96	0.20	0.58	0.62	0.60	1135	678.76	
0.64	0.13	0.57	0.60	0.59	604	678.44	
0.32	0.07	0.54	0.56	0.55	201	678.12	
0.00	0.00	0.49	0.49	0.49	0	677.80	



Discharge Coefficient Table Tullis et al. (1995)

	Angle wall makes with centerline α										
	6	8	12	15	18	25	35	90			
A0	0.49	0.49	0.49	0.49	0.49	0.49	0.49	0.49			
A1	-0.24	1.08	1.06	1.00	1.32	1.51	1.69	1.46			
A2	-1.20	-5.27	-4.43	-3.57	-4.13	-3.83	-4.05	-2.56			
A3	2.17	6.79	5.18	3.82	4.24	3.40	3.62	1.44			
A4	-1.03	-2.83	-1.97	-1.38	-1.50	-1.05	-1.10				

LABYRINTH WEIR DESIGN No Approach Velocity

 PROJECT:
 Tobacco Labyrinth
 TIME:
 14:12:19

 PROJECT NO.
 2002879
 DATE:
 13-Jul-20

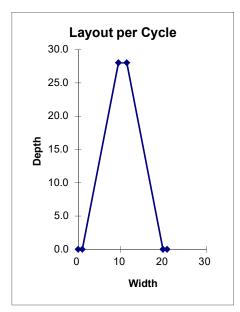
 FLOOD CRITERIA:
 1/2 PMF
 BY:
 PDD

USER INPUT									
Max. Res	Zr	681.0 ft	Thickness						
Crest el.	Zc	677.8 ft	Wall	Tw	1.25	ft			
Floor el.	Zf	673.0 ft	Slab	Ts	1.25	ft			
Spillway width	Ws	125.0 ft	Cutoff Depth						
Apex Width	2a	2 ft	Sheet Pile	Ds	1	ft			
No. of cycles	n	6	Conc Wall	Dc	1	ft			
Magnification	L/W	3							

Note: L_{de}/B must be <= 0.35 Ho/P must be <= 0.9 α must be >= 6 deg

CREST	LAYOUT
	(One Cycle)

	X	Y
9.42 28.0° 11.42 28.0° 19.83 0	0	0
11.42 28.0° 19.83 0	1.00	0
19.83 0	9.42	28.01
	11.42	28.01
20.83 0	19.83	0
	20.83	0



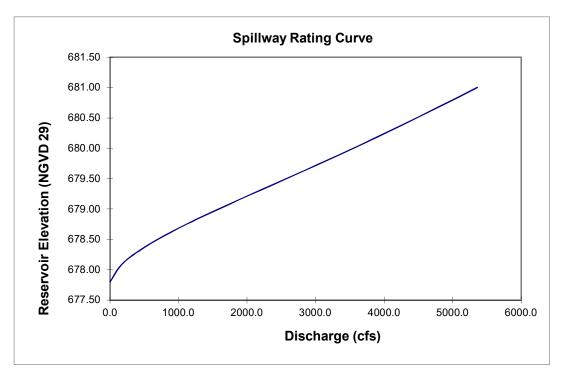
<u>LABYRINTH DIMENSIONS (Per Cycle)</u> Wall Height P 4.8 **ft** 20.83 **ft** Width W Length L 62.50 ft Wall Length В 29.25 ft Depth D 28.01 **ft** Head max Н 3.20 ft Wall Angle α 16.72 deg Length of 8.21 ft Interference

DISCHARGE
Qmax 5,360 cfs

COEFFICIENTS	_
Column	4.00
Cd lower	0.43
Cd Upper	0.49
Cd	0.47
Efficacy	1.86

RATING CURVE

HEAD	H _o /P	\mathbf{C}_{lower}	C_{upper}	\mathbf{C}_{d}	Q	RES	
3.20	0.67	0.43	0.49	0.47	5360	681.00 1/2 PMF EI.	
2.88	0.60	0.45	0.52	0.49	4792	680.68	
2.56	0.53	0.48	0.54	0.51	4218	680.36	
2.24	0.47	0.50	0.57	0.54	3625	680.04	
1.92	0.40	0.53	0.59	0.56	3009	679.72	
1.60	0.33	0.55	0.61	0.58	2374	679.40	
1.28	0.27	0.57	0.62	0.60	1739	679.08	
0.96	0.20	0.58	0.62	0.60	1135	678.76	
0.64	0.13	0.57	0.60	0.59	604	678.44	
0.32	0.07	0.54	0.56	0.55	201	678.12	
0.00	0.00	0.49	0.49	0.49	0	677.80	



Discharge Coefficient Table Tullis et al. (1995)

	Angle wall makes with centerline α										
	6	8	12	15	18	25	35	90			
A0	0.49	0.49	0.49	0.49	0.49	0.49	0.49	0.49			
A1	-0.24	1.08	1.06	1.00	1.32	1.51	1.69	1.46			
A2	-1.20	-5.27	-4.43	-3.57	-4.13	-3.83	-4.05	-2.56			
A3	2.17	6.79	5.18	3.82	4.24	3.40	3.62	1.44			
A4	-1.03	-2.83	-1.97	-1.38	-1.50	-1.05	-1.10				



710.0

710.5

711.0

711.5

712.0

712.5

713.0

713.5

15.2

15.7

16.2

16.7

17.2

17.7

18.2

18.7

1.38

1.43

1.47

1.52

1.56

1.61

1.65

1.70

1.05

1.05

1.06

1.06

1.07

1.07

1.07

1.07

Client:	Four Lakes Task Force	Project #:	2002879	Page:	
Project:	Smallwood Dam	Ву:	PDD	Date:	6/19/2020
Subject:	Rating Curve Calculations	Checked:	RJA	Date:	7/13/2020
		Approved:	WHW	Date:	7/13/2020

Ogee Spillway Discharge Rating Curve - Tainter Gates (Fully Open)

2 Gates

Input Parameter Gate 1 Gate 2 Unit Reference: 23.4 feet Crest Length 23.4 STID, rev 2018 Crest El. 694.8 694.8 NGVD29 feet STID, rev 2018 Ogee Design Head (Ho) 11 11 feet from Upper Nappe Profile Tab 672.6 672.6 Original Drawings, Drw 10418 Apron Elevation Approach Depth (P) 22.2 22.2 feet Number of Piers 1 1 -Discharge, $Q = Leff*C*H^{3/2}$ Abutment coeff (Ka) 0.1 0.1 -Pier coeff (Kp) 0 0 L=L'- 2 (NKP +Ka) He Top of Non-Overflow El. 715.7 715.7 feet P/Ho 2.02 2.02 Design Head Coeff. 3.92 3.92 Figure 9-23 USBR DOSD 1987

Reservoir El.	Total Head, He	He / Ho	Ratio of Coeff. c/co	Adjusted Coeff., c	Eff. Length (Gate 1)	Eff. Length (Gate 2)	Discharge (Gate 1)	Discharge (Gate 2)	Discharge (Both Gates)
ft	ft	-	-	-	ft	ft	cfs	cfs	cfs
694.8	0.0	0.00	0.78	3.07	23.4	23.4	0	0	0
695.0	0.2	0.02	0.79	3.09	23.4	23.4	6	6	13
695.5	0.7	0.06	0.81	3.16	23.3	23.3	43	43	86
696.0	1.2	0.11	0.82	3.22	23.2	23.2	98	98	196
696.5	1.7	0.15	0.84	3.28	23.1	23.1	167	167	335
697.0	2.2	0.20	0.85	3.33	23.0	23.0	249	249	499
697.5	2.7	0.25	0.86	3.38	22.9	22.9	343	343	686
698.0	3.2	0.29	0.87	3.43	22.8	22.8	446	446	893
698.5	3.7	0.34	0.89	3.47	22.7	22.7	560	560	1,119
699.0	4.2	0.38	0.90	3.51	22.6	22.6	682	682	1,364
699.5	4.7	0.43	0.91	3.55	22.5	22.5	813	813	1,625
700.0	5.2	0.47	0.92	3.59	22.4	22.4	951	951	1,903
700.5	5.7	0.52	0.92	3.62	22.3	22.3	1,098	1,098	2,195
701.0	6.2	0.56	0.93	3.66	22.2	22.2	1,251	1,251	2,502
701.5	6.7	0.61	0.94	3.69	22.1	22.1	1,411	1,411	2,823
702.0	7.2	0.65	0.95	3.72	22.0	22.0	1,578	1,578	3,157
702.5	7.7	0.70	0.96	3.75	21.9	21.9	1,752	1,752	3,503
703.0	8.2	0.75	0.96	3.78	21.8	21.8	1,931	1,931	3,862
703.5	8.7	0.79	0.97	3.81	21.7	21.7	2,116	2,116	4,232
704.0	9.2	0.84	0.98	3.83	21.6	21.6	2,307	2,307	4,613
704.5	9.7	0.88	0.98	3.86	21.5	21.5	2,503	2,503	5,005
705.0	10.2	0.93	0.99	3.89	21.4	21.4	2,704	2,704	5,408
705.5	10.7	0.97	1.00	3.91	21.3	21.3	2,910	2,910	5,820
706.0	11.2	1.02	1.00	3.94	21.2	21.2	3,121	3,121	6,243
706.5	11.7	1.06	1.01	3.96	21.1	21.1	3,337	3,337	6,674
707.0	12.2	1.11	1.02	3.98	21.0	21.0	3,557	3,557	7,115
707.5	12.7	1.15	1.02	4.01	20.9	20.9	3,782	3,782	7,564
708.0	13.2	1.20	1.03	4.03	20.8	20.8	4,010	4,010	8,021
708.5	13.7	1.25	1.03	4.05	20.7	20.7	4,243	4,243	8,485
709.0	14.2	1.29	1.04	4.07	20.6	20.6	4,478	4,478	8,957
709.5	14.7	1.34	1.04	4.09	20.5	20.5	4,717	4,717	9,435

4.11

4.13

4.15

4.16

4.18

4.19

4.20

4.21

20.4

20.3

20.2

20.1

20.0

19.9

19.8

19.7

20.4

20.3

20.2

20.1

20.0

19.9

19.8

19.7

4,959

5,203

5,449

5,697

5,945

6,194

6,442

6,689

4,959

5,203

5,449

5,697

5,945

6,194

6,442

6,689

9,918

10,406

10,898

11,393

11,890

12,387

12,884

13,379

Weir Flow

LABYRINTH WEIR DESIGN No Approach Velocity

PROJECT: Smallwood Labyrinth

TIME: 14:12:19 PROJECT NO. 2002879 DATE: 13-Jul-20 FLOOD CRITERIA: 1/2 PMF PDD BY:

		USER	INPUT_			
Max. Res	Zr	713.5 ft	Thickness			
Crest el.	Zc	709.5 ft	Wall	Tw	1.25	ft
Floor el.	Zf	703.5 ft	Slab	Ts	1.25	ft
Spillway width	Ws	125.0 ft	Cutoff Depth			
Apex Width	2a	2 ft	Sheet Pile	Ds	1	ft
No. of cycles	n	6	Conc Wall	Dc	1	ft
Magnification	L/W	3				

CHECK ON RATIOS

 $Lde/B = \overline{0.35}$ **USE FEWER CYCLES** $H_o/P = 0.67$ Ho/P RATIO IS OK $\alpha = 16.72$ Angle IS OK

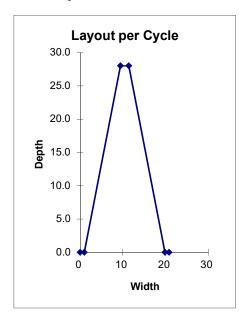
Note: L_{de}/B must be <= 0.35 Ho/P must be <= 0.9 α must be >= 6 deg

LABYRINTH DIME	ENSIONS (Per Cycle)	
Wall Height	Р	6 ft
Width	W	20.83 ft
Length	L	62.50 ft
_ Wall Length	В	29.25 ft
Depth	D	28.01 ft
Head max	Н	4.00 ft
Wall Angle	α	16.72 deg
Length of	L_{de}	10.26 ft
Interference		

CREST LAYOUT

(One Cycle)

X	Υ
0	0
1.00	0
9.42	28.01
11.42	28.01
19.83	0
20.83	0

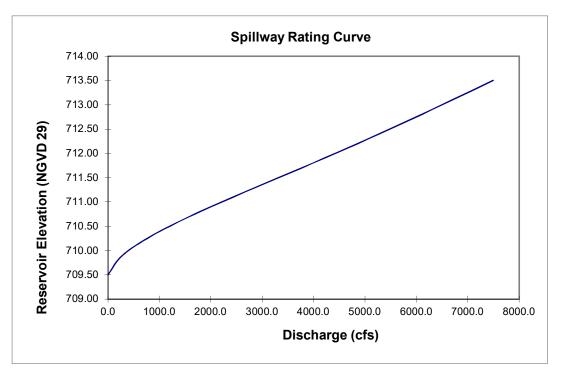


DISCHARGE Qmax 7,491 **cfs**

COEFFICIENTS	_
Column	4.00
Cd lower	0.43
Cd Upper	0.49
Cd	0.47
Efficacy	1.86

RATING CURVE

HEAD	H _o /P	\mathbf{C}_{lower}	\mathbf{C}_{upper}	\mathbf{C}_{d}	Q	RES	
4.00	0.67	0.43	0.49	0.47	7491	713.50 1/2 PMF EI.	
3.60	0.60	0.45	0.52	0.49	6697	713.10	
3.20	0.53	0.48	0.54	0.51	5895	712.70	
2.80	0.47	0.50	0.57	0.54	5066	712.30	
2.40	0.40	0.53	0.59	0.56	4205	711.90	
2.00	0.33	0.55	0.61	0.58	3318	711.50	
1.60	0.27	0.57	0.62	0.60	2431	711.10	
1.20	0.20	0.58	0.62	0.60	1586	710.70	
0.80	0.13	0.57	0.60	0.59	844	710.30	
0.40	0.07	0.54	0.56	0.55	281	709.90	
0.00	0.00	0.49	0.49	0.49	0	709.50	



Discharge Coefficient Table Tullis et al. (1995)

			Angle wa	ıll makes	with cent	erline α		
	6	8	12	15	18	25	35	90
A0	0.49	0.49	0.49	0.49	0.49	0.49	0.49	0.49
A1	-0.24	1.08	1.06	1.00	1.32	1.51	1.69	1.46
A2	-1.20	-5.27	-4.43	-3.57	-4.13	-3.83	-4.05	-2.56
A3	2.17	6.79	5.18	3.82	4.24	3.40	3.62	1.44
A4	-1.03	-2.83	-1.97	-1.38	-1.50	-1.05	-1.10	



Client:	Four Lakes Task Force	Project #:	2002879	Page:	
Project:	Secord Dam	Ву:	PDD	Date:	6/19/2020
Subject:	Rating Curve Calculations	Checked:	RJA	Date:	7/13/2020
		Approved:	WHW	Date:	7/13/2020

Ogee Spillway Discharge Rating Curve - Tainter Gates (Fully Open)

Input Parameter	Gate #1	Gate#2	Unit	Reference:
Crest Length	23	23	feet	Spicer Group Hydraulic Report
Crest El.	737.5	737.5	NGVD29 feet	Spicer Group Hydraulic Report
Ogee Design Head (Ho)	15	15	feet	from Upper Nappe Profile Tab
	702.8	702.8		
Approach Depth (P)	34.7	34.7	feet	
Number of Piers	1	1	-	Discharge, $Q = Leff^*C^*H^{3/2}$
Abutment coeff (Ka)	0.1	0.1	-	
Pier coeff (Kp)	0	0		
Top of Non-Overflow El.	757.8	757.8	feet	L=L'- 2 (NKP +Ka) He
P/Ho	2.31	2.31		
Design Head Coeff.	3.92	3.92	Figure 9-23	USBR DOSD 1987

	Weir Flow													
Reservoir Fl.	Total Head, He	He / Ho	Ratio of Coeff.	Adjusted Coeff.,	Eff. Length	Eff. Length	Discharge	Discharge	Discharge (All					
neservon zn	Total fieda, fie	110 / 110	c/co	С	(Gate 1)	(Gate 2)	(Gate 1)	(Gate 2)	Gates)					
ft	ft	-	-	-	ft	ft	cfs	cfs	cfs					
750.8	13.3	0.89	0.99	3.87	20.3	20.3	3,814	3,814	7,628					
751.0	13.5	0.90	0.99	3.87	20.3	20.3	3,900	3,900	7,80					
751.5	14.0	0.93	0.99	3.89	20.2	20.2	4,119	4,119	8,237					
752.0	14.5	0.97	1.00	3.91	20.1	20.1	4,340	4,340	8,680					
752.5	15.0	1.00	1.00	3.93	20.0	20.0	4,565	4,565	9,130					
753.0	15.5	1.03	1.01	3.95	19.9	19.9	4,793	4,793	9,585					
753.5	16.0	1.07	1.01	3.96	19.8	19.8	5,023	5,023	10,047					
754.0	16.5	1.10	1.01	3.98	19.7	19.7	5,257	5,257	10,514					
754.5	17.0	1.13	1.02	4.00	19.6	19.6	5,493	5,493	10,986					
755.0	17.5	1.17	1.02	4.01	19.5	19.5	5,732	5,732	11,463					

	New Auxiliary Spillway									
		Spillway Length Discharge								
Pond El. (ft)	Invert El. (ft)	(ft)	С	Head (ft)	(cfs)					
755	752	200	3.3	3	3,429					

Attachment 3 – OPCC Estimate Worksheets – ½ PMF

OPINION OF PROBABLE COST - CONCEPTUAL Project: Sanford Dam Client: Four Lakes Task Force (FLTF) Design Discharge = 1/2 PMF

Project No.: 2002879
Date: 6/30/2020
Estimated by: P. Drew / R. Anderson
Checked by: B. Walton

<u>Item</u>	<u>Description</u>	Quantity	<u>Units</u>		Unit Price	<u>Total Cost</u>	<u>Notes</u>
0.00	General Conditions	4	1.0	•	4.004.000	A 004 000	70/ -4 Oth Cot-
0.01 0.02	Contractor Mobilization / Demobilization Bonds and Insurance	1	LS LS	\$	4,081,000 1,166,000	\$ 4,081,000 \$ 1,166,000	7% of Other Costs 2% of Other Costs
0.03	Construction Permits	1	LS	\$	50,000		270 Of Other Codes
					Subtotal	\$ 5,297,000	
.00	Site Preparation						
1.01	Erosion and Sediment Control	1	LS	\$	50,000	\$ 50,000	
1.02	Temporary Access Roads, Facilities and Laydown Areas	1	LS	\$		\$ 500,000	
1.03	Stabilize Breach Channel and Right Embankment	1	LS	\$		\$ 300,000	PS-27.5 SSP, circular cells, D=35', B=31.5', H=45'. Cofferdam L=500', \$40/sf
1.04	Phase I Cofferdams - Spillway and PH Area (U/S and D/S)	1	LS	\$	4,120,000	\$ 4,120,000	installed; ASTM C-33 fill at \$20/cy
1.05	Phase II Cofferdams - Aux Spillway Area	1	LS	\$	6,590,000	\$ 6,590,000	PS-27.5 SSP, circular cells, D=35', B=31.5', H=45'. Cofferdam L=800', \$40/sf
1.06	Construction Dewatering	1	LS	\$	2,000,000		installed; ASTM C-33 fill at \$20/cy \$1M / year x 2 years
1.07	Sediment Removal and Dredging	1	LS	\$	700,000		······ /··· - /··
					Subtotal	\$ 14,260,000	
.00	Demolition / Abandonment						
2.01	Powerhouse Decommission, Demolition and Disposal	1	LS	\$	2,000,000	\$ 2,000,000	
2.02	Gated Spillway Demolition and Disposal	1	LS	\$		\$ 2,000,000	
2.03	Embankment Excavation and Disposal Mechanical and Electrical Equipment Demolition and Disposal	50,000 1	CY LS	\$		\$ 1,000,000 \$ 250,000	
				_		\$ 5,250,000	
3.01	Left Abutment / Embankment Reconstruction	13,300	CY	\$	30	\$ 399,000	
3.02	Sheet Pile Cutoff	8,000	SF	\$		\$ 560,000	PZC-18 hot-rolled or equal with treated interlocks, L = 40' avg
3.03	Erosion Protection	2,000	CY	\$	80	\$ 160,000	, ,
					Subtotal	\$ 1,119,000	
00	Right Embankment Reconstruction						
4.01	Sheet Pile Cutoffs	70,200	SF	\$		\$ 6,318,000	PZC-26 hot-rolled or equal with treated interlocks, L = 60' avg
4.02	Embankment Fill	226,400	CY	\$		\$ 6,792,000	20' wide crest, 2.5H:1V U/S and D/S slopes, crest EL. 638, L = 1170'
4.03 4.04	Structural Fill Filter Sand and Drainage Stone Layers	0 44,500	CY CY	\$		\$ - \$ 1,780,000	under labyrinth spillway but not main body of flanking embankments C-33 Filter sand and minus 1/2" drainage stone
4.04	Upstream Rip-Rap Protection	9,100	CY	\$		\$ 1,780,000	3' layer of Medium Riprap over 12" bedding stone down to El. 610
4.06	Downstream Rip-Rap Protection	7,000	CY	\$		\$ 560,000	3' layer of Heavy Riprap over 12" bedding stone
4.07 4.08	Bedding Stone Crest Gravel	5,400 0	CY	\$		\$ 243,000 \$ -	12" thick layer of bedding stone on U/S and D/S slopes 6" thick layer of MNDOT granular base course over 20' wide crest
4.09	Topsoil, Seed and Temp Erosion Protection	0	SY	\$		\$ -	included under site restoration
	' '					\$ 16,421,000	
00	Now Catad Spillway / Outlet Works						
5.01	New Gated Spillway / Outlet Works Reinforced Concrete Ogee and Base Slab	1,500	CY	\$	900	\$ 1,350,000	
5.02	Reinforced Concrete Structure Piers and Walls	830	CY	\$	1,200		
5.03	Reinforced Concrete Stilling Basin Floor Slabs	2,200	CY	\$		\$ 1,760,000	
5.04 5.05	Reinforced Concrete Stilling Basin Side Walls Mass Concrete	1,100 5,900	CY CY	\$		\$ 1,320,000 \$ 3,540,000	Foundation slab
5.06	Crest Gates (Shallow) - Installed with Hoists and Controls	4	EA.	\$	300,000		\$850 / sf gate area> 22' wide x 11' high> 242 sf / gate x \$850 = \$205,700
3.00	Clest Gates (Ghallow) - Installed with Holsts and Controls	4	LA	Ψ	300,000	1,200,000	gate. Too low use \$300k
5.07	Crest Gates (Deep) - Installed with Hoists and Controls	2	EA	\$	500,000	\$ 1,000,000	\$850 / sft gate area> 22' wide x 20' high> 440 sf /gate x \$850 = \$374,000 gate. Too low, use \$500k
5.08	Sheet Pile Cutoffs	24,000	SF	\$	90		PZC-26 SSP, L = 30' under walls at all 4 sides
5.09	Steel Frame Operators Deck	1	LS	\$	2,000,000 _ Subtotal	\$ 2,000,000 \$ 15,326,000	
					Subtotal	13,320,000	
00	New Labyrinth Spillway Structure						
6.01 6.02	Reinforced Concrete Labyrinth Floor Slabs Reinforced Concrete Chute Slabs	670 830	CY	\$ \$		\$ 603,000 \$ 664,000	
6.03	Reinforced Concrete Crute Stabs Reinforced Concrete Stilling Basin Floor Stabs	980	CY	\$		\$ 664,000 \$ 784,000	
6.04	Reinforced Concrete End Sill	100	CY	\$		\$ 150,000	
6.05	Reinforced Concrete Labyrinth Weir Walls	170	CY	\$		\$ 238,000	
6.06	Reinforced Concrete Spillway and Stilling Basin Walls	250	CY	\$		\$ 300,000	L= 50' under upstream end of labyrinth floor slab; L = 25' under D/S under of
6.07	Steel Sheet Pile Cutoffs	13,400	SF	\$		\$ 1,206,000	stilling basin and wing walls; PZC-26 SSP
6.08	Upstream Riprap	1,000	CY	\$		\$ 80,000	3' layer of medium riprap over 12" bedding stone down to EL. 610
6.09 6.10	Downstream Heavy Riprap Apron and Chute Bedding	3,700 1,000	CY CY	\$ \$		\$ 296,000 \$ 45,000	3' layer of heavy riprap over 12" bedding stone 12" thick layer of bedding stone on U/S slope and D/S apron and chute
6.11	Structural Fill	17,200	CY	\$	35		.2 alian layer or bodding storic on 0/0 stope and 0/0 aproil and triute
6.12	Filter Sand and Drainage Stone	4,600	CY	\$	40		
6.13	Drain Pipe (Solid and Slotted)	1,000	LF	\$	25	\$ 25,000	8" slotted schedule 80 drain pipe, 3 transverse slotted pipes plus 2 solid outle pipes to D/S
6.14	Pre-Engineered Pedestrian Bridge and Piers (access over stilling basin)	1	LS	\$	500,000	\$ 500,000	pipes to Dio
	,					\$ 5,677,000	
00	Site Restoration						
7.01	Place Overburden, Seed, Fertilize, and Mulch Slopes	1	LS	\$	100,000	\$ 100,000	
7.02	Downstream River Restoration	1	LS	\$	100,000	\$ 100,000	
7.03	Dam Safety Monitoring Instrumentation	1	LS	\$		\$ 50,000	
					Subtotal	\$ 250,000	
	Subtotal					\$ 63,600,000	
	Contingency					\$ 19,080,000	
	Construction Subtotal					\$ 82,680,000	
	Engineering Investigations, Design and Construction Engineering	_	_		10%	\$ 8,268,000	
	Engineering investigations, Design and Constitution Engineering	-	-		1070	\$ 8,268,000	
	Total Estimated Cost					\$ 90,948,000	
					say	\$ 90,948,000	
					Juy	, 30,040,000	
	n presented on this sheet represents our opinion of probable costs in 2020						
	g judgment, and/or published cost data. Client administrative/engineering pased on contractor's perceived risk, site access, season, market conditior						
	esed or implied.	, o.o. 140 W	11105			, 5, 55555 produttou fiorelli	
	:						

OPINION OF PROBABLE COST - CONCEPTUAL Project No.: 2002879 Project: Edenville Dam Client: Four Lakes Task Force (FLTF) Date: 6/30/2020 Design Discharge = 1/2 PMF Estimated by: P. Drew / R. Anderson Checked by: B. Walton **Total Cost** Description Quantity Units **Unit Price** Notes .00 General Conditions 0.01 Contractor Mobilization / Demobilization LS 9.495.000 9,495,000 7% of Other Costs LS \$ 2,713,000 Bonds and Insurance 2,713,000 2% of Other Costs 0.03 Construction Permits LS 50.000 50.000 12,258,000 Subtotal 1.00 Site Preparation 1.01 Erosion and Sediment Control 50,000 500,000 50.000 LS 1.02 Temporary Access Roads, Facilities and Laydown Areas LS 500,000 1.04 Stabilize Breach Channel and Edenville Dam Left Embankment LS 500,000 500,000 PS-27.5 SSP, circular cells, D=40', B=35', H=50'. Cofferdam L= 780' (L=2200' 1.05 Phase I Cofferdams - Edenville Spillway, PH and Breach Area LS \$ 19,950,000 19.950.000 perim), \$40/sf installed; ASTM C-33 fill at \$20/cy PS-27.5 SSP, circular cells, D=35', B=31.5', H=45'. Cofferdam L=250' (500' Phase II Cofferdam - Tobacco Spillway Area LS \$ 4,120,000 1.06 tot), \$40/sf installed; ASTM C-33 fill at \$20/cy 4,120,000 1.07 Construction Dewatering LS \$ 3.000.000 3.000.000 \$1M / year x 3 years 1,500,000 Sediment Removal and Dredging LS 1,500,000 1.08 1.09 River Diversion LS \$ 2.000.000 2.000.000 Stream diversion during phase 1 and 2 Subtotal 31,620,000 2.00 M-30 Diversion Multiple Bay Box Culvert Structure with Sufficient Capacity for both the 2.01 Temporary Diversion Control Structure Upstream of Tobacco Dam LS \$ 2,000,000 1 2.000.000 Tittabawassee and Tobacco Rivers LS 2,000,000 2 000 000 Remove diversion structure and reconstruct causeway bridge 2.02 Remove M-30 Control Structure and Restore Causeway Bridge 1 \$ Subtotal \$ 4,000,000 Demolition / Abandonment 2,500,000 2,500,000 3.01 Edenville Powerhouse Decommissioning, Demolition and Disposal 3.02 Edenville Gated Spillway Demolition and Disposal LS \$ 1 500 000 \$ 1 500 000 Tobacco Gated Spillway Demolition and Disposal LS 3.03 1,500,000 1,500,000 3.04 Mechanical and Electrical Equipment Demolition and Disposal LS \$ 250,000 250.000 Subtotal 5,750,000 4.00 Edenville Embankments - Reconstruct Breached Section PZC-26 hot-rolled or equal with treated interlocks, from left abutment to M-30, 4.01 Sheet Pile Cutoffs 50,800 SF \$ 90 \$ 4.572.000 L ssp = 80' avg, L emb = 635' 20' wide crest, 2.5H:1V U/S and D/S slopes, crest EL. 685, L emb = 635' Embankment Fill 216 900 CY 30 6,507,000 4 02 \$ \$ CY \$ 4.03 Structural Fill 0 \$ 35 under labyrinth spillway but not main body of flanking embankments C-33 Filter sand and minus 1/2" drainage stone
3' layer of Medium Riprap over 12" bedding stone from EL. 685 down to 650 4.04 Filter Sand and Drainage Stone Layers 31,500 CY \$ 1,260,000 4.05 Upstream Riprap Protection 6,600 CY \$ 80 528,000 3' layer of Heavy Riprap over 12" bedding stone from EL. 650 to 627 12" thick layer of bedding stone on U/S and D/S slopes 4.06 4.07 Downstream Riprap Protection 4,400 CY CY 80 \$ 352,000 \$ Bedding Stone 4.000 45 180,000 4.08 Crest Gravel 200 CY 35 \$ 7,000 6" thick layer of MNDOT granular base course over 20' wide crest 4.09 Topsoil, Seed and Temporary Erosion Protection 0 SY \$ included under site restoration Subtotal 13,406,000 Edenville Embankments - Repaired and Stabilized Section PZC-26 hot-rolled or equal with treated interlocks, from left abutment to M-30, 5.01 Sheet Pile Cutoffs 227,200 SF \$ 90 \$ 20,448,000 L = 80' avg 5.02 Embankment Fill 149,500 CY \$ 30 4,485,000 20' wide crest, 2.5H:1V U/S and D/S slopes, crest EL. 685, L = 2840' \$ \$ \$ 5.03 Structural Fill CY 35 under labyrinth spillway but not main body of flanking embankments Filter Sand and Drainage Stone Layers 5.04 42 900 CY \$ 40 1 716 000 C-33 Filter sand and minus 1/2" drainage stone 3' layer of Medium Riprap over 12" bedding stone from EL. 685 to 650 CY \$ Upstream Riprap Protection 29,700 80 2,376,000 5.05 3' layer of Heavy Riprap over 12" bedding stone from EL. 650 to 627 12" thick layer of bedding stone on U/S and D/S slopes under riprap 5.06 Downstream Riprap Protection 19 600 CY \$ 80 \$ 1,568,000 CY Bedding Stone 45 5.07 16,400 738,000 5 08 Crest Gravel
Topsoil, Seed and Temporary Erosion Protection 1,100 CY \$ 35 2 \$ 39,000 6" thick layer of MNDOT granular base course over 20' wide crest included under site restoration 5.09 \$ 31.370.000 Subtotal Tobacco Embankments - Repaired and Stabilized Section 6.00 PZC-26 hot-rolled or equal with treated interlocks, from right abutment to M-6.01 Sheet Pile Cutoffs 144,000 SF \$ 90 \$ 12,960,000 30, L = 60' avg 20' wide crest, 2.5H:1V U/S and D/S slopes, crest EL. 685, L = 2400' 126,300 30 3,789,000 6.02 Embankment Fill CY \$ \$ CY \$ under labyrinth spillway but not main body of flanking embankments C-33 Filter sand and minus 1/2" drainage stone 3' layer of Medium Riprap over 12" bedding stone from EL. 685 to 650 6.03 Structural Fill 0 \$ 35 36,300 CY 1,452,000 Filter Sand and Drainage Stone Layers \$ 6.05 Upstream Riprap Protection 25.100 80 2.008.000 CY 16,500 \$ 1,320,000 3' layer of Heavy Riprap over 12" bedding stone from EL. 650 to 627 6.06 Downstream Riprap Protection 80 6.07 Bedding Stone 13,900 \$ 45 \$ 625,500 12" thick layer of bedding stone on U/S and D/S slopes under riprap CY 35 \$ 31,500 6" thick layer of MNDOT granular base course over 20' wide crest Topsoil, Seed and Temporary Erosion Protection 6.09 0 SY \$ included under site restoration 22.186.000 Subtotal **7.00** New Gated Spillways and Outlet Works - Edenville Apportioned from Sanford quantities (L = 90') \$850 / sf gate area --> 24' wide x 11' high --> 264 sf / gate x \$850 = \$224,400 7.01 Edenville 3-Bay Spillway Structure FΔ 5.043.000 \$ 5.043.000 7.02 Crest Gates (Shallow) - Installed with Hoists and Controls 2 EΑ 300,000 \$ 600,000 \$ gate. Too low use \$300k \$850 / sft gate area --> 24' wide x 20' high --> 480 sf /gate x \$850 = \$408,000 Crest Gates (Deep) - Installed with Hoists and Controls 1 EΑ \$ 500.000 \$ 500.000 7.03 / gate. Too low, use \$500k PZC-26 SSP, L = 30' under walls at all 4 sides Sheet Pile Cutoffs 10,800 SF 90 972,000 7.04

Steel Frame Operators Deck

7.05

750,000

Subtotal

750,000 **7,865,000** Apportioned from Sanford (L = 100')

EΑ

OPINION OF PROBABLE COST - CONCEPTUAL Project No.: 2002879 Project: Edenville Dam Client: Four Lakes Task Force (FLTF) Date: 6/30/2020 Design Discharge = 1/2 PMF Estimated by: P. Drew / R. Anderson Checked by: B. Walton Item Description Quantity Units **Unit Price Total Cost** Notes .00 New Gated Spillways and Outlet Works - Tobacco 8.01 Tobacco 3-Bay Spillway Structure ΕA 5.043.000 \$ 5.043.000 Apportioned from Sanford quantities (L = 90') \$850 / sf gate area --> 24' wide x 11' high --> 264 sf / gate x \$850 = \$224,400 2 EΑ 300.000 \$ 8.02 Crest Gates (Shallow) - Installed with Hoists and Controls \$ 600.000 gate. Too low use \$300k \$850 / sft gate area --> 24' wide x 20' high --> 480 sf /gate x \$850 = \$408,000 8.03 Crest Gates (Deep) - Installed with Hoists and Controls 1 EΑ \$ 500.000 \$ 500.000 / gate. Too low, use \$500k PZC-26 SSP, L = 30' under walls at all 4 sides 8.04 Sheet Pile Cutoffs 10,800 SF 90 972,000 8.05 Steel Frame Operators Deck EΑ \$ 750,000 750.000 Apportioned from Sanford (L = 100') 7,865,000 Subtotal \$ New Labyrinth Spillway Structure - Edenville Reinforced Concrete Labyrinth Floor Slabs 9.00 Reinforced Concrete Labyrinth Flo Reinforced Concrete Chute Slabs 900 459,000 930 CY 744.000 9.02 \$ 800 \$ CY 9.03 Reinforced Concrete Stilling Basin Floor Slabs 740 800 592,000 9.04 Reinforced Concrete End Sill 70 \$ 1.500 \$ 105.000 Reinforced Concrete Labyrinth Weir Walls \$ \$ 1,400 9.06 Reinforced Concrete Spillway and Stilling Basin Walls 250 CY 1,200 300,000 PZC-26 SSP w/ Wadit; L= 50' under upstream end of labyrinth floor slab; L = Steel Sheet Pile Cutoffs SF 9.07 12,400 \$ 90 \$ 1,116,000 25' under D/S under of stilling basin and wing walls
3' layer of medium riprap over 12" bedding stone down to EL. 650 9.08 Upstream Riprap 900 CY 80 \$ 72,000 \$ Downstream Heavy Riprap Apron and Chute 5' layer of heavy riprap over 12" bedding stone 12" thick layer of bedding stone on U/S and D/S apron and chute 9.09 3.100 CY \$ 80 \$ 248,000 9.10 Bedding 900 CY 45 40,500 Structural Fill 9.11 25.100 CY 35 \$ 878.500 9.12 Filter Sand and Drainage Stone 5,500 CY 40 220,000 8" slotted schedule 80 drain pipe, 3 transverse slotted pipes plus 2 solid outlet 9.13 Drain Pipe (Solid and Slotted) 600 LF \$ 25 \$ 15,000 Pre-Engineered Pedestrian Bridge and Piers (access over stilling basin 9.14 1 LS \$ 500,000 \$ 500,000 Subtotal 5,542,000 0.00 New Labyrinth Spillway Structure - Tobacco Reinforced Concrete Labyrinth Floor Slabs Reinforced Concrete Chute Slabs 10.01 510 CY CY 900 459.000 930 800 744,000 10.02 CY 10.03 Reinforced Concrete Stilling Basin Floor Slabs 740 ลกก \$ 592,000 Reinforced Concrete End Sill 105,000 10.04 70 1,500 10.05 Reinforced Concrete Labyrinth Weir Walls 180 CY \$ 1 400 \$ 252 000 Reinforced Concrete Spillway and Stilling Basin Walls 250 CY 1,200 300,000 10.06 PZC-26 SSP w/ Wadit; L= 50' under upstream end of labyrinth floor slab; L = 12,400 SF \$ 90 \$ 1,116,000 10.07 Steel Sheet Pile Cutoffs 25' under D/S under of stilling basin and wing walls 72 000 10.08 Upstream Riprap 900 CY \$ 80 \$ 3' layer of medium riprap over 12" bedding stone down to EL. 610 5' layer of heavy riprap over 12" bedding stone 10.09 Downstream Heavy Riprap Apron and Chute 3,100 CY 80 248,000 Bedding Structural Fill 10.10 900 CY \$ 45 \$ 40.500 12" thick layer of bedding stone on U/S and D/S apron and chute CY 35 878,500 25,100 10.11 10.12 Filter Sand and Drainage Stone 5,500 CY \$ 40 \$ 220,000 8" slotted schedule 80 drain pipe, 3 transverse slotted pipes plus 2 solid outlet 10.13 Drain Pipe (Solid and Slotted) 600 LF \$ 25 \$ 15.000 pipes to D/S Pre-Engineered Pedestrian Bridge and Piers (access over stilling basin LS 10.14 1 500,000 500,000 Subtotal 5.542.000 1.00 Site Restoration Place Overburden, Seed, Fertilize, and Mulch Slopes 11.01 LS 300,000 300,000 Tobacco and Tittabawassee River D/S Restoration LS 200.000 11 03 Dam Safety Monitoring Instrumentation LS 100 000 \$ 100 000 \$ 500.000 Subtotal Subtotal \$ 147 904 000 30%

8%

say

44,371,000 **192.275.000**

15,382,000

207,657,000 207,657,000

nformation presented on this sheet represents our opinion of probable costs in 2020 dollars. Unit and lump-sum prices are based on costs for imilar projects, engineering judgment, and/or published cost data. Client administrative/engineering costs and regulatory fees not included. Actual bids and total project costs may vary based on contractor's perceived risk, site access, season, market conditions, etc. No warranties concerning the accuracy of costs presented herein are expressed or implied.

Contingency
Construction Subtotal

Total Estimated Cost

Engineering Investigations, Design and Construction Engineering

PINION OF PROBABLE COST - CONCEPTUAL PINION OF PRUBABLE COC.

Project: Smallwood Dam

Client: Four Lakes Task Force (FLTF) Project No.: 2002879 Date: 6/30/2020 Estimated by: P. Drew / R. Anderson Checked by: B. Walton Item Description Quantity Units Unit Price Total Cost 585,000 167,000 \$ 50,000 \$ 167,000 LS LS Subtotal 1.00 1.0' Site Preparation
Erosion and Sediment Control
Temporary Access Roads, Facilities and Laydown 20.000 \$ 20 000 1 02 LS \$ 100,000 \$ 100,000 Assume reservoir is drawn down - no cofferdam needed to construct 1.05 Cofferdams - Aux Spillway 0 LS the Auxiliary Spillway Not required for Auxiliary Spillway construction since impounment is 1.07 LS Construction Dewatering drawn down Dredge material from tailrace 150,000 Sediment Removal and Dredging 150,000 1.08 LS 1.09 River Diversion LS Assume reservoir is drawn down 270.000 Subtotal Powerhouse Decommissioning and TG Abandon Smallwood Powerhouse Decommissioning and TG Remove turbine-generator set and all associated electrical and mechanical controls related to generation 2.01 LS \$ 500,000 \$ 500.000 \$ 500.000 Subtotal Left Embankment Repair and Stabilization 90 \$ 30 \$ 40 \$ widen crest from 15' to 20' wide, provide 2.5H:1V D/S slopes C-33 Filter sand and minus 1/2" drainage stone 5,100 3,100 CY CY Filter Sand and Drainage Stone Layers 3.03 124,000 3' layer of Medium Riprap over 12" bedding stone from EL. 716 to 3.04 Upstream Riprap Protection 2.500 CY \$ 80 \$ 200.000 3.05 Downstream Riprap Protection 2 900 CY \$ 80 \$ 232 000 3' layer of Heavy Riprap over 12" bedding stone from EL. 700 to 675 3.06 Bedding Stone 1.800 CY 45 s 81.000 12" thick layer of bedding stone on U/S and D/S slopes under riprag Crest Gravel
Topsoil, Seed and Temporary Erosion Protection 3.07 120 CY 35 2 \$ 4,000 6" thick layer of MNDOT granular base course over 20' wide crest included under site restoration \$ 794,000 Right Embankment Repair and Stabilization 4.00 4.01 4.02 Sheet Pile Cutoffs Already has SSP cutoff widen crest from 15' to 20' wide, provide 2.5H:1V D/S slopes SF CY 90 30 40 \$ 2,400 72,000 C-33 Filter sand and minus 1/2" drainage stone 3' layer of Medium Riprap over 12" bedding stone from EL. 716 to 4.03 Filter Sand and Drainage Stone Lavers 1.500 CY 60.000 Upstream Riprap Protection 4.04 1.200 CY \$ 80 \$ 96,000 4.05 Downstream Riprap Protection 1.300 CY \$ 80 \$ 104.000 3' layer of Heavy Riprap over 12" bedding stone from EL. 700 to 675 Bedding Stone Crest Gravel Topsoil, Seed and Temporary Erosion Protection 12" thick layer of bedding stone on U/S and D/S slopes under riprap 6" thick layer of MNDOT granular base course over 20' wide crest included under site restoration 4.06 4.07 4.08 830 60 0 45 35 37,000 2,000 371,000 Gated Spillway Rehabilitation 5.00 250.000 250.000 same unit costs at Edenville and Sanford cellular concrete - 1000 psi minimum foundation underpinning to support additional concrete weight; 150 kigh design capacity / pile supplemental D/S riprap in the talirace area 5.02 New Crest Gates - Installed with Hoists and Controls EA CY 300,000 \$ 600.000 5.03 750 450,000 5.04 Foundation Micropiles and Structural Pile Caps 24 ΕA 20,000 \$ 480,000 100,000 \$ Subtotal \$ 100,000 Downstream Tailrace Armoring 5.05 LS 6.00 Powerhouse Rehabilitation

Misc surface concrete and masonry repairs 100,000 \$ 100,000 6.02 Convert water passages to low level outlet EΑ 500.000 \$ 500.000 Includes wicket gate conversion and controls for low level outlet includes whoket gate conversion and controls for low level outlet cellular concrete - 1000 psi minimum foundation underpinning to support additional concrete weight; 150 kip design capacity / pile 6.03 Concrete Backfill 300 CY 600 \$ 180,000 6 04 Foundation Micropiles and Structural Pile Caps 9 FΑ \$ 20.000 \$ 180 000 Subtotal s 960 000 New Labyrinth Spillway Structure
Reinforced Concrete Labyrinth Floor Slabs
Reinforced Concrete Chute Slabs 560 CY 448,000 7.03 Reinforced Concrete Stilling Basin Floor Slabs 560 CY CY 800 \$,500 \$ 448,000 Reinforced Concrete End Sill 7.04 80 1.500 120.000 Reinforced Concrete Labyrinth Weir Walls Reinforced Concrete Spilllway and Stilling Basin Walls 7.05 7.06 140 CY 1,400 \$ 1,200 \$ 196,000 276,000 230 PZC-26 SSP w/ Wadit; L= 40' under upstream end of labyrinth floor slab; L = 20' under D/S under of stilling basin and wing walls 7.07 Steel Sheet Pile Cutoffs 7,500 SF \$ 90 \$ 675,000 3' layer of medium riprap over 12" bedding stone down to EL. 690 5' layer of heavy riprpap over 12" bedding stone 12" thick layer of bedding sone on U/S and D/S apron and chute Upstream Riprap Downstream Heavy Riprap Apron and Chute 44,800 2,320 80 45 185,600 7.09 7.10 CY CY \$ \$ \$ Bedding 750 33,750 7.11 Structural Fill 9,260 CY 35 324,100 7.12 Filter Sand and Drainage Stone 5.600 CY 40 224.000 8" slotted schedule 80 drain pipe, 2 transverse slotted pipes and 3 7.13 Drain Pipe (Solid and Slotted) 470 ΙF \$ 25 S 11.750 solid outlet pipes Pre-Engineered Pedestrian Bridge and Piers (access over stilling basin) LS 500,000 \$ Not required since apron is above TW \$ 3,446,000 Subtotal Place Overburden, Seed, Fertilize, and Mulch Slopes Dam Safety Monitoring Instrumentation 100,000 130.000 Subtotal 9.153.000 Subtotal Contingency
Construction Subtotal 30% 2,746,000 Engineering Investigations, Design and Construction Engineering **Total Estimated Cost** \$ 13.684.000 say \$ 13.684.000 Information presented on this sheet represents our opinion of probable costs in 2020 dollars. Unit and lump-sum prices are based en costs for similar projects, engineering judgment, and/or published cost data. Client administrative/engineering costs and regulatory fees not included. Actual bids and total project costs may vary based on contractor's perceived risk, site access, season, market conditions, etc. No warranties concerning the accuracy of costs presented herein are expressed or implied.

PINION OF PROBABLE COST - CONCEPTUAL PINION OF PRUBABLE - Project: Secord Dam
Client: Four Lakes Task Force (FLTF) Project No.: 2002879 Date: 6/30/2020 Estimated by: P. Drew / R. Anderson Checked by: B. Walton Item Description Units Unit Price ,044,000 298,000 LS LS 298,000 50,000 <u>\$</u> 0.03 Construction Permits 50,000 1.392.000 Subtotal 1.01 Site Preparation ent Contr 1.01 1.02 1.05 1.07 1.08 Temporary Access Roads, Facilities and Laydown Areas 200,000 200,000 LS LS LS LS Assume reservoir is drawn down - no cofferdam needed to construct the Auxiliary Spillway Not required for Auxiliary Spillway construction since impoundment is drawn down Dredge material from tailrace Cofferdams Construction Dewatering Sediment Removal and Dredging 1.09 River Diversion Assume reservoir is drawn down \$ 220,000 Subtotal Powerhouse Decommissioning and TG Abandonment 2.00 Remove turbine-generator set and all associated electrical and mechanical controls related to generatio 500,000 **500,000** Subtotal Left Embankment Repair and Stabilization 90 30 40 80 PZC-26 hot-rolled or equal with treated interlocks, L = 60' avg widen crest from 15' to 20' wide, provide 2.5H:1V D/S slopes C-33 Filter sand and minus 1/2" drainage stone 3.01 3.02 Sheet Pile Cutoffs Embankment Fill 28,200 4,600 2,538,000 138,000 CY CY CY CY CY CY CY Filter Sand and Drainage Stone Layers 104,000 3.03 2,600 3.04 Upstream Riprap Protection 3.700 296,000 3' laver of Medium Riprap over 12" bedding stone 3 layer of Heavy Riprap over 12" bedding stone 12" thick layer of bedding stone on U/S and D/S slopes under riprap 6" thick layer of MMDOT granular base course over 20" wide crest included under site restoration 3.05 Downstream Riprap Protection 2,100 80 168,000 Bodding Stone
Crest Gravel
Topsoil, Seed and Temporary Erosion Protection 90,000 3.06 2,000 2.00 3,341,000 Right Embankment Repair and Stabilization 4.00 PZC-26 hot-rolled or equal with treated interlocks, L = 60' avg 21,600 90 1,944,000 4.02 Embankment Fill 3.600 CY 30 40 80 108.000 widen crest from 15' to 20' wide, provide 2.5H:1V D/S slope widen crest from 15' to 20' wide, provide 2.5H:1V D/S slopes C-33 Filter sand and minus 1/2" drainage stone 3' layer of Medium Riprap over 12" bedding stone 3' layer of Heavy Riprap over 12" bedding stone 12" thick layer of bedding stone on U/S and D/S slopes under riprap 6" thick layer of MNDOT granular base course over 20' wide crest included under site restoration Filter Sand and Drainage Stone Layers
Upstream Riprap Protection
Downstream Riprap Protection
Bedding Stone 4.03 2.000 80,000 CY CY CY CY CY SY 2,800 1,600 1,500 100 224,000 128,000 67,500 3,500 4 04 4.04 4.05 4.06 4.07 4.08 35 \$ 2.00 \$ Crest Gravel
Topsoil, Seed and Temporary Erosion Protection 2,555,000 5.01 Gated Spillway Rehabilitation 250.000 250.000 Misc. surface concrete repairs and modifications Structural Concrete - Ogee Structural Concrete - Side Walls and Piers New Hydraulic Crest Gates - Installed with Hoists and Controls Concrete Backfill 1,200 1,200 500,000 600 CY CY EA CY EA LS 168.000 360,000 1,000,000 720,000 600,000 2 1,200 cellular concrete - 1000 psi minimum foundation underpinning to support additional concrete weight; 150 kip design capacity / pile supplemental D/S riprap in the tailrace area Foundation Micropiles and Structural Pile Caps Downstream Tailrace Armoring 20,000 5.06 5.07 30 200,000 200,000 **3,298,000** Subtotal Powerhouse Rehabilitation Misc. surface concrete and masonry repairs Convert water passages to low level outlet Concrete Backfill Foundation Micropiles and Structural Pile Caps EA CY EA Includes wicket gate conversion and controls for low level outlet cellular concrete - 1000 psi minimum foundation underpinning to support additional concrete weight; 150 kip design capacity / pile 600 20,000 Subtotal 7.00 New Overflow Auxiliary Spillway Structure Reinforced Concrete Floor Slabs 300 900 270.000 Reinforced Concrete Chute Slabs Reinforced Concrete Stilling Basin Floor Slabs Reinforced Concrete Stilling Basin Floor Slabs Reinforced Concrete Spillway and Stilling Basin Walls 590 300 92 CY CY CY 7.02 800 472.000 1,200 110,000 PZC-18 SSP w/ Wadit; L= 30° under upstream end of labyrinth floor slab; L = 20° under D/S under of stilling basin and wing walls; L = 30° along D/S toe of left embankment 7.05 Steel Sheet Pile Cutoffs 16,000 SF 70 \$ 1,120,000 Upstream Riprap 700 80 80 56.000 7.06 7.07 CY CY CY CY CY LF LS 3' layer of medium riprap over 12" bedding stone 3' layer of riprap over 12" bedding stone Downstream Heavy Riprap Apron 176.000 2.200 7.08 Downstream Riprap Conveyance Channel 3,100 1,800 80 248,000 \$ \$ \$ \$ \$ 7.09 Bedding Structural Fill 45 81.000 12" thick layer of bedding stone on U/S and D/S apron and chute 7.10 7.11 7.12 7.13 0 1,000 600 35 40 25 Filter Sand and Drainage Stone
Drain Pipe (Solid and Slotted)
Sacrificial Culvert Bridge to Parking Area 40 000 8" slotted schedule 80 drain pipe 100,000 100,000 2,928,000 Subtotal Site Restoration
Place Overburden, Seed, Fertilize, and Mulch Slopes
Dam Safety Monitoring Instrumentation LS 30.000 \$ 30,000 Subtotal 130,000 16,310,000 Subtotal Contingency
Construction Subtotal 30% 4,893,000 21,203,000 Engineering Investigations, Design and Construction Engineering 15% \$ 3.180.000

24,383,000

say \$

Total Estimated Cost

Information presented on this sheet represents our opinion of probable costs in 2020 dollars. Unit and lump-sum prices are based on costs for similar projects, engineering judgment, and/or published cost data. Client administrative/engineering costs and regulatory fees not included. Actual bids and total project costs may vary based on contractor's perceived risk, site access, season, market conditions, etc. No warranties concerning the accuracy of costs presented herein are expressed or implied.

Attachment 4 – OPCC Estimate Worksheets – PMF

OPINION OF PROBABLE COST - CONCEPTUAL
Project: Sanford Dam
Client: Four Lakes Task Force (FLTF)
Design Discharge = PMF

Project No.: 2002879
Date: 6/30/2020
Estimated by: P. Drew / R. Anderson
Checked by: B. Walton

					Спескей by: В. wa	ton	
Item	Description	Quantity	Units		Unit Price	Total Cost	Notes
0.00	General Conditions	<u> </u>	<u> </u>		<u> </u>	10101 0001	110100
0.01	Contractor Mobilization / Demobilization	1	LS	\$	5,682,000 \$	5,682,000	7% of Other Costs
0.02	Bonds and Insurance	1	LS	\$	1,624,000 \$	1,624,000	2% of Other Costs
0.03	Construction Permits	1	LS	\$	50,000 \$	50,000	
					Subtotal \$	7,356,000	
.00	Site Preparation						
1.01	Erosion and Sediment Control	1	LS	\$	50,000 \$	50,000	
1.02	Temporary Access Roads, Facilities and Laydown Areas	1	LS	\$	500,000 \$	500,000	
1.03	Stabilize Breach Channel and Right Embankment	1	LS	\$	300,000 \$	300,000	Double the size of the Phase I Cofferdam. Increase the Crest gates from 6 t
1.04	Phase I Cofferdams - Spillway and PH Area (U/S and D/S)	1	LS	\$	8,240,000 \$	8,240,000	12.
1.05	Dhana II Coffeedana Avy Cailly ay Area	1	1.0	•	0.005.000	0.005.000	Increase the size of the Phase II Cofferdam. Increase labyrinth spillway from
	Phase II Cofferdams - Aux Spillway Area		LS	\$	9,985,000 \$	9,985,000	165 feet to 250 feet.
1.06	Construction Dewatering	1	LS	\$	2,000,000 \$	2,000,000	
1.07	Sediment Removal and Dredging	1	LS	\$	700,000 \$ Subtotal \$	700,000 21,775,000	
					oubtotu. V	21,110,000	
.00	Demolition / Abandonment						
2.01	Powerhouse Decommission, Demolition and Disposal	1	LS	\$	2,000,000 \$	2,000,000	
2.02	Gated Spillway Demolition and Disposal Embankment Excavation and Disposal	1 50,000	LS CY	\$ \$	2,000,000 \$ 20 \$	2,000,000 1,000,000	
2.03	Mechanical and Electrical Equipment Demolition and Disposal	1	LS	\$	250,000 \$	250,000	
					Subtotal \$	5,250,000	
.00	Left Abutment Reconstruction (L = 200 feet)	12.000	01/	•	00 0	000.000	
3.01 3.02	Left Abutment / Embankment Reconstruction Sheet Pile Cutoff	13,000 8,000	CY SF	\$ \$	30 \$ 70 \$	390,000 560,000	
3.02	Erosion Protection	2,000	CY	\$	80 \$	160,000	
2.30		_,000	٥.	•	Subtotal \$	1,110,000	
.00	Right Embankment Reconstruction (L = 935 feet)						
4.01	Sheet Pile Cutoffs Embankment Fill	56,000 181,000	SF	\$	90 \$	5,040,000	Reduced the embankment reconstruction length from 1,170 to 935 feet
4.02 4.03	Structural Fill	181,000 0	CY CY	\$ \$	30 \$ 35 \$	5,430,000	
4.04	Filter Sand and Drainage Stone Layers	36,000	CY	\$	40 \$	1,440,000	
4.05	Upstream Rip-Rap Protection	7,000	CY	\$	80 \$	560,000	
4.06	Downstream Rip-Rap Protection	6,000	CY	\$	80 \$	480,000	
4.07	Bedding Stone	4,000	CY	\$	45 \$	180,000	
4.08 4.09	Crest Gravel Topsoil, Seed and Temp Erosion Protection	0	CY SY	\$ \$	35 \$ 2 \$		
	Toposii, ooda ana Tomp Erddion Totodion	ŭ	٠.	•	Subtotal \$	13,130,000	
.00	New Gated Spillway / Outlet Works						
5.01 5.02	Reinforced Concrete Ogee and Base Slab Reinforced Concrete Structure Piers and Walls	3,000	CY CY	\$ \$	900 \$ 1,200 \$	2,700,000	Double the size of the new gated spillway
5.02	Reinforced Concrete Stilling Basin Floor Slabs	1,700 4,400	CY	\$	800 \$	2,040,000 3,520,000	
5.04	Reinforced Concrete Stilling Basin Side Walls	2,200	CY	\$	1,200 \$	2,640,000	
5.05	Mass Concrete	11,800	CY	\$	600 \$	7,080,000	
5.06	Crest Gates (Shallow) - Installed with Hoists and Controls	8	EA	\$	300,000 \$	2,400,000	
5.07 5.08	Crest Gates (Deep) - Installed with Hoists and Controls Sheet Pile Cutoffs	4 48,000	EA SF	\$ \$	500,000 \$ 90 \$	2,000,000 4,320,000	
5.09	Steel Frame Operators Deck	1	LS	\$	4,000,000 \$	4,000,000	
				•	Subtotal \$	30,700,000	
.00	New Labyrinth Spillway Structure	1.000	CV	Φ.	000 €	000 000	Increase the Johnwinth millions from 405 feet to 250 feet
6.01 6.02	Reinforced Concrete Labyrinth Floor Slabs Reinforced Concrete Chute Slabs	1,000 1,300	CY CY	\$ \$	900 \$ 800 \$	900,000 1,040,000	Increase the labyrinth spillway from 165 feet to 250 feet
6.03	Reinforced Concrete Stilling Basin Floor Slabs	1,500	CY	\$	800 \$	1,200,000	
6.04	Reinforced Concrete End Sill	150	CY	\$	1,500 \$	225,000	
6.05	Reinforced Concrete Labyrinth Weir Walls	300	CY	\$	1,400 \$	420,000	
6.06 6.07	Reinforced Concrete Spillway and Stilling Basin Walls Steel Sheet Pile Cutoffs	400 20.300	CY SF	\$ \$	1,200 \$ 90 \$	480,000 1,827,000	
6.08	Upstream Riprap	20,300 1,500	CY	\$	90 \$ 80 \$	1,827,000	
6.09	Downstream Heavy Riprap Apron and Chute	5,600	CY	\$	80 \$	448,000	
6.10	Bedding	1,500	CY	\$	45 \$	68,000	
6.11	Structural Fill	26,100	CY	\$	35 \$	914,000	
6.12 6.13	Filter Sand and Drainage Stone Drain Pipe (Solid and Slotted)	7,000 1,500	CY LF	\$ \$	40 \$ 25 \$	280,000 38,000	
6.14	Pre-Engineered Pedestrian Bridge and Piers (access over stilling basin	1,500	LF	\$	1,000,000 \$	1,000,000	
	5 - State (•	Subtotal \$	8,960,000	
		4	10	•	100.000	400.000	
	Site Restoration	1	LS	\$ \$	100,000 \$ 100,000 \$	100,000 100,000	
7.01	Place Overburden, Seed, Fertilize, and Mulch Slopes	1		Ψ			
		1	LS LS	\$	50,000 \$	50,000	
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration				50,000 \$ Subtotal \$	250,000	
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration						
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration						
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency				Subtotal \$	250,000 88,531,000 26,559,000	
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal				Subtotal \$	250,000 88,531,000	
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency Construction Subtotal				\$ subtotal \$ \$ 30% \$ \$ \$ \$	250,000 88,531,000 26,559,000 115,090,000	
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency				Subtotal \$	250,000 88,531,000 26,559,000	
7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency Construction Subtotal				\$ subtotal \$ \$ 30% \$ \$ \$ \$	250,000 88,531,000 26,559,000 115,090,000	
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency Construction Subtotal				\$ subtotal \$ \$ 30% \$ \$ \$ \$	250,000 88,531,000 26,559,000 115,090,000	
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency Construction Subtotal Engineering Investigations, Design and Construction Engineering				Subtotal \$ 30% \$ 10% \$	250,000 88,531,000 26,559,000 115,090,000 11,509,000 126,599,000	
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency Construction Subtotal Engineering Investigations, Design and Construction Engineering				Subtotal \$ 30% \$ \$ \$ 10% \$	250,000 88,531,000 26,559,000 115,090,000 11,509,000	
7.01 7.02	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency Construction Subtotal Engineering Investigations, Design and Construction Engineering				Subtotal \$ 30% \$ 10% \$	250,000 88,531,000 26,559,000 115,090,000 11,509,000 126,599,000	
7.01 7.02 7.03	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency Construction Subtotal Engineering Investigations, Design and Construction Engineering Total Estimated Cost	-	LS -	\$	Subtotal \$ 30% \$ 10% \$ say \$	250,000 88,531,000 26,559,000 115,090,000 11,509,000 126,599,000 126,599,000	
7.01 7.02 7.03	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency Construction Subtotal Engineering Investigations, Design and Construction Engineering	1 - 20 dollars. Ur	LS - nit and lur	\$ mp-su	Subtotal \$ 30% \$ 10% \$ say \$	250,000 88,531,000 26,559,000 115,090,000 11,509,000 126,599,000 126,599,000	
7.01 7.02 7.03	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency Construction Subtotal Engineering Investigations, Design and Construction Engineering Total Estimated Cost on presented on this sheet represents our opinion of probable costs in 20 engineering judgment, and/or published cost data. Client administrative/sists may vary based on contractor's perceived risk, site access, season, if	1 - 20 dollars. Ur engineering co	LS - - sit and lur	mp-su egula	Subtotal \$ 30% \$ 10% \$ say \$ m prices are based o tory fees not included	250,000 88,531,000 26,559,000 115,090,000 11,509,000 126,599,000 126,599,000 n costs for similar Actual bids and total	
7.01 7.02 7.03	Place Overburden, Seed, Fertilize, and Mulch Slopes Downstream River Restoration Dam Safety Monitoring Instrumentation Subtotal Contingency Construction Subtotal Engineering Investigations, Design and Construction Engineering Total Estimated Cost on presented on this sheet represents our opinion of probable costs in 20 engineering judgment, and/or published cost data. Client administrative/	1 - 20 dollars. Ur engineering co	LS - - sit and lur	mp-su egula	Subtotal \$ 30% \$ 10% \$ say \$ m prices are based o tory fees not included	250,000 88,531,000 26,559,000 115,090,000 11,509,000 126,599,000 126,599,000 n costs for similar Actual bids and total	

OPINION OF PROBABLE COST - CONCEPTUAL Project No.: 2002879 Project: Edenville Dam Client: Four Lakes Task Force (FLTF) Date: 6/30/2020 Design Discharge = PMF Estimated by: P. Drew / R. Anderson Checked by: B. Walton Description Item Quantity Units **Unit Price Total Cost** Notes .00 General Conditions 0.01 Contractor Mobilization / Demobilization LS 11.377.000 11.377.000 7% of Other Costs Bonds and Insurance LS 3,251,000 \$ 3,251,000 2% of Other Costs 0.03 Construction Permits LS \$ 50,000 50.000 Subtotal 1.00 Site Preparation 1.01 1.02 Erosion and Sediment Control 50,000 500,000 50.000 LS \$ Temporary Access Roads, Facilities and Laydown Areas LS 500,000 1.04 Stabilize Breach Channel and Edenville Dam Left Embankment LS 500,000 500,000 1.05 Phase I Cofferdams - Edenville Spillway, PH and Breach Area LS 3.940.000 23.940.000 Increase the size of the Phase I Cofferdam by 20% Double the size of the Phas II Cofferdam 8,240,000 Construction Dewatering Sediment Removal and Dredging 1 07 LS \$ \$ 3 000 000 \$ 3 000 000 LS 1,500,000 1,500,000 1.09 River Diversion LS \$ 2.000.000 2.000.000 Subtotal 39,730,000 M-30 Diversion 2.00 Temporary Diversion Control Structure Upstream of Tobacco Dam Remove M-30 Control Structure and Restore Causeway Bridge 2,000,000 2,000,000 2.02 LS 2,000,000 \$ 2,000,000 Subtotal \$ 4,000,000 .00 Demolition / Abandonment 2.500.000 3.01 Edenville Powerhouse Decommissioning, Demolition and Disposal LS 2.500.000 3.02 Edenville Gated Spillway Demolition and Disposal LS 1,500,000 \$ 1,500,000 3.03 Tobacco Gated Spillway Demolition and Disposal LS \$ \$ 1.500.000 1.500.000 Mechanical and Electrical Equipment Demolition and Disposal 250,000 **5,750,000** 3.04 LS 250,000 \$ \$ Subtotal .00 Edenville Embankments - Reconstruct Breached Section (L = 635 feet) 50.800 4.01 Sheet Pile Cutoffs 90 4.572.000 30 6,507,000 216,900 \$ \$ \$ \$ \$ CY 4.03 Structural Fill 0 \$ 35 4.04 Filter Sand and Drainage Stone Layers 31,500 CY 40 1,260,000 6.600 4.05 Upstream Riprap Protection \$ 80 528.000 CY 4.06 Downstream Riprap Protection 4 400 80 352,000 4.07 \$ Bedding Stone 4.000 45 180,000 35 7,000 Topsoil, Seed and Temporary Erosion Protection 4.09 0 SY \$ 2 Subtotal 13.406.000 .00 Edenville Embankments - Repaired and Stabilized Section (Unbreached - L = 2, 40 feet) 5.01 211 200 SF 90 \$ \$ 19 008 000 Reduced the embankment reconstruction length from 2,840 to 2,640 feet 30 5.02 **Embankment Fill** CY 4,167,000 138,900 CY 5.03 Structural Fill 'n 35 \$ \$ \$ \$ \$ \$ \$ 5.04 Filter Sand and Drainage Stone Layers 39,900 1,596,000 5.05 Upstream Riprap Protection 27.600 CY \$ \$ 80 2.208.000 CY Downstream Riprap Protection 1,456,000 5.06 18,200 80 5.07 **Bedding Stone** 15.300 CY 45 689,000 \$ 1,000 CY 35 Crest Gravel 35,000 5.08 5.09 Topsoil, Seed and Temporary Erosion Protection n SY \$ Subtotal 29,159,000 .00 Tobacco Embankments - Repaired and Stabilized Section (L=2,200 feet) 11.880.000 Reduced the embankment reconstruction length from 2,400 to 2,220 feet 6.01 132,000 90 115,800 30 3,474,000 \$ \$ \$ \$ \$ \$ 6.03 Structural Fill 0 CY \$ 35 Filter Sand and Drainage Stone Layers CY CY CY CY 6.04 33,200 40 1,328,000 6.05 Upstream Riprap Protection 23.000 80 1.840.000 Downstream Riprap Protection 15,200 80 1,216,000 6.07 Bedding Stone 13.200 45 \$ 594.000 6.08 800 CY 35 28,000 Topsoil, Seed and Temporary Erosion Protection 6.09 0 SY 2 Subtotal 20,360,000 .00 New Gated Spillways and Outlet Works - Edenville 7.01 EΑ 5.043.000 10.086.000 Doubled the size of the Gated Spillway Edenville 3-Bay Spillway Structure Crest Gates (Shallow) - Installed with Hoists and Controls 7.02 EΑ 300,000 \$ 1,200,000 7.03 7.04 Crest Gates (Deep) - Installed with Hoists and Controls Sheet Pile Cutoffs EA SF 500,000 \$ 1.000.000 21,600 1,944,000 90 1,500,000 **15,730,000** 7.05 Steel Frame Operators Deck EΑ 1.500.000 Subtotal 8.00 New Gated Spillways and Outlet Works - Tobacco Doubled the size of the Gated Spillway 8.01 Crest Gates (Shallow) - Installed with Hoists and Controls 8.02 EΑ 300.000 \$ 1.200.000 8.03 Crest Gates (Deep) - Installed with Hoists and Controls EΑ 500,000 1,000,000 8.04 Sheet Pile Cutoffs 21,600 SF 90 \$ 1.944.000 8.05 ĒΑ 15.730.000 Subtotal

OPINION OF PROBABLE COST - CONCEPTUAL Project No.: 2002879 Project: Edenville Dam Client: Four Lakes Task Force (FLTF) Date: 6/30/2020 Design Discharge = PMF Estimated by: P. Drew / R. Anderson Checked by: B. Walton Item Description Quantity Units **Unit Price Total Cost** Notes .00 New Labyrinth Spillway Structure - Edenville 9.01 900 720.000 Increase spillway width from 125 feet to 200 feet 800 Reinforced Concrete Chute Slabs 1,500 CY 1,200,000 9.02 9.03 9.04 Reinforced Concrete Stilling Basin Floor Slabs Reinforced Concrete End Sill CY 960,000 165,000 1,200 800 \$ 110 1,500 Reinforced Concrete Labyrinth Weir Walls
Reinforced Concrete Spillway and Stilling Basin Walls CY CY 9.05 300 1 400 \$ \$ \$ \$ \$ \$ \$ \$ 420 000 1,200 480,000 9.06 9.07 Steel Sheet Pile Cutoffs 19.800 SF 90 1.782.000 1,400 80 112,000 Upstream Riprap CY CY CY CY 9.08 Downstream Heavy Riprap Apron and Chute 9 09 5 000 80 400.000 Bedding Structural Fill 45 63,000 1,400 9.10 9.11 40,200 35 1,407,000 9.12 Filter Sand and Drainage Stone 8,800 40 352,000 Drain Pipe (Solid and Slotted)
Pre-Engineered Pedestrian Bridge and Piers (access over stilling basin 9.13 LF LS 25 \$ 24.000 1,000,000 Subtotal 9.085.000 0.00 New Labyrinth Spillway Structure - Tobacco 10.01 900 720.000 Increase spillway width from 125 feet to 200 feet Reinforced Concrete Chute Slabs 10.02 1,500 CY 800 \$ 1,200,000 Reinforced Concrete Stilling Basin Floor Slabs 10.03 1.200 CY 800 960,000 \$ \$ \$ \$ \$ \$ \$ \$ \$ \$ CY CY CY SF 10.04 Reinforced Concrete End Sill 110 1,500 165,000 Reinforced Concrete Labyrinth Weir Walls Reinforced Concrete Spillway and Stilling Basin Walls Steel Sheet Pile Cutoffs 10.05 300 1.400 420,000 10.06 400 1,200 480,000 19.800 1.782.000 10.07 90 10.08 1,400 CY 80 112,000 400,000 Downstream Heavy Riprap Apron and Chute 10.09 5,000 80 Bedding 10.10 1,400 CY 45 35 63,000 1,407,000 Structural Fill 40,200 10.11 10.12 Filter Sand and Drainage Stone 8,800 CY LF 40 \$ 352,000 Drain Pipe (Solid and Slotted) 10.13 960 25 \$ 24.000 Pre-Engineered Pedestrian Bridge and Piers (access over stilling basin LS 1,000,000 Subtotal \$ 9.085.000 11.00 Site Restoration Place Overburden, Seed, Fertilize, and Mulch Slopes 11.01 300,000 \$ 300,000 Tobacco and Tittabawassee River D/S Restoration LS LS 200,000 \$ 200.000 Dam Safety Monitoring Instrumentation 11.03 100.000 500,000 \$ Subtotal Subtotal 177,213,000 Contingency
Construction Subtotal 30% 53,164,000 **230,377,000** Engineering Investigations, Design and Construction Engineering 8% 18,430,000 **Total Estimated Cost** \$ 248,807,000 say \$ 248,807,000 nformation presented on this sheet represents our opinion of probable costs in 2020 dollars. Unit and lump-sum prices are based on costs for similar projects, engineering judgment, and/or published cost data. Client administrative/engineering costs and regulatory fees not included. Actual bids and total project costs may vary based on contractor's perceived risk, site access, season, market conditions, etc. No warranties concerning the accuracy of costs presented herein are expressed or implied.

OPINION OF PROBABLE COST - CONCEPTUAL Project: Smallwood Dam Client: Four Lakes Task Force (FLTF) Project No.: 2002879 Date: 6/30/2020 Estimated by: P. Drew / R. Anderson Checked by: B. Walton Design Discharge = PM Description Quantity Units Unit Price Total Cost Item 7% of Other Costs 2% of Other Costs 590,000 \$ 590,000 Bonds and Insurance LS 0.03 Construction Permits LS 50,000 \$ 50,000 Subtotal 2.704.000 Site Preparation 1.00 1.01 Frosion and Sediment Control LS 20.000 \$ 20.000 1.02 Temporary Access Roads, Facilities and Laydown Areas LS \$ 100.000 \$ 100.000 1.05 Phase I Cofferdams -Gated Spillway, PH LS Phase I Cofferdam selected apportioned from Tobacco Spillway 6,867,000 \$ 6,867,000 Construction Dewatering 1.07 0 LS 1.08 Sediment Removal and Dredging LS LS 150.000 \$ 150.000 1.09 River Diversion 7,137,000 2.00 Powerhouse Decommissioning and TG Abandonment Costs from Edenville Dam Powerhouse Demolition Smallwood Powerhouse Decommissioning, Demolition and Dis Smallwood Gated Spillway Demolition and Disposal Mechanical and Electrical Equipment Demolition and Disposal LS LS 1,500,000 250,000 \$ 2.03 250,000 4,250,000 Subtotal Left Embankment Repair and Stabilization (L = 325 feet) .00 90 \$ 30 \$ 3.02 Embankment Fill 5.100 CY 153.000 3.03 Filter Sand and Drainage Stone Layers CY 40 \$ 124.000 Upstream Riprap Protection 2,500 CY \$ 80 \$ 200,000 3.04 3.05 Downstream Riprap Protection 2.900 CY \$ 80 \$ 232.000 3.06 Bedding Stone 1.800 CY 45 \$ 81.000 3.07 Crest Gravel 120 35 4,000 Topsoil, Seed and Temporary Erosion Protection \$ 794.000 Subtotal Right Embankment Repair and Stabilization (L = 100 feet) .00 Reduced the embankment rehabilitation length from 150 to 100 fee 4.01 Embankment Fill 48.000 4.02 1.600 CY 30 \$ 40 \$ 4.03 Filter Sand and Drainage Stone Layers 1.000 CY 40.000 4.04 Upstream Riprap Protection 800 CY 80 \$ 64,000 CY 4.05 900 80 72,000 4.06 Bedding Stone 600 CY 45 \$ 35 \$ 27.000 4.07 Crest Gravel 40 0 CY SY 1,000 opsoil, Seed and Temporary Erosion Protection 252,000 5.00 5.0 New Gated Spillway and Outlet Works 8,405,000 1,200,000 New Gated spillway. Cost apportioned from Edenville Dar Sanford 5-Bay Spillway Structure
Crest Gates (Shallow) - Installed with Hoists and Controls 5.02 Crest Gates (Deep) - Installed with Hoists and Controls EΑ 5.03 500,000 500,000 5.04 Sheet Pile Cutoffs 10,800 SF EA 90 972,000 Steel Frame Operators Deck 1.000.000 6.00 Powerhouse Rehabilitation EA EA CY 100.000 Powerhouse rehabilitation costs removed. Convert water passages to low level outlet Concrete Backfill 500,000 \$ 600 \$ Foundation Micropiles and Structural Pile Caps EΑ 20,000 \$ 6.04 Subtotal \$ -New Labyrinth Spillway Structure (L = 180 ft) 7.00 630,000 Increase spillway width from 125 feet to 180 feet Reinforced Concrete Chute Slabs 7.02 800 CY CY CY CY SF CY CY 800 640.000 7.03 7.04 7.05 Reinforced Concrete Stillling Basin Floor Slabs Reinforced Concrete End Sill Reinforced Concrete Labyrinth Weir Walls 800 100 200 800 1,500 1,400 640,000 150,000 280,000 Reinforced Concrete Spilllway and Stilling Basin Walls 7.06 300 1.200 360.000 7.07 Steel Sheet Pile Cutoffs 10.800 90 80 972,000 800 3,300 1,100 Upstream Riprap
Downstream Heavy Riprap Apron and Chute
Bedding
Structural Fill 64,000 264,000 7.09 7.10 80 45 49,500 7.11 13.000 CY 35 455.000 7.12 Filter Sand and Drainage Stone CY. 40 324.000 Drain Pipe (Solid and Slotted) 25 \$ 17,500 700 Pre-Engineered Pedestrian Bridge and Piers (access over stilling 7.14 0 LS \$ 500,000 \$ \$ 4,846,000 Subtotal Place Overburden, Seed, Fertilize, and Mulch Slopes
Dam Safety Monitoring Instrumentation LS 30,000 \$ 30,000 Subtotal 130.000 32,190,000 Contingency
Construction Subtotal 30% 9,657,000 **41.847.000** Engineering Investigations, Design and Construction Engineering 15% 6.277.000

48,124,000

48.124.000

say \$

Information presented on this sheet represents our opinion of probable costs in 2020 dollars. Unit and lump-sum prices are based on costs for similar projects, engineering judgment, and/or published cost data. Client administrative/engineering costs and regulatory fees not included. Actual bids and total project costs may vary based on contractor's perceived risk, site access, season, market conditions, etc. No warranties concerning the accuracy of costs presented herein are expressed or implied.

Total Estimated Cost

Project: Secord Dam Client: Four Lakes Task Force (FLTF) Project No.: 2002879 Date: 6/30/2020 Design Discharge = PM Estimated by: P. Drew / R. Anderson Item Quantity Units Total Cost General Conditions Contractor Mobilization / Demobilization Bonds and Insurance LS LS LS 2,363,000 675,000 7% of Other Costs 2% of Other Costs 50,000 <u>\$</u> Construction Permits 50,000 **3,088,000** Subtotal Site Preparation 1.00 Erosion and Sediment Control Temporary Access Roads, Facilities and Laydown Areas LS LS LS 20,000 20,000 200,000 6,867,000 6,867,000 1.05 1.07 Cofferdams Construction Dewatering Sediment Removal and Dredging 0 LS LS 1.09 River Diversion 7.087.000 Subtotal 2.00 Powerhouse Decommissioning and TG Abandonment 2,500,000 \$ 1,500,000 \$ 250,000 \$ **ubtotal** \$ Costs from Edenville Dam Powerhouse Demolition 2,500,000 1,500,000 Secord Powerhouse Decommissioning, Demolition and Dispos Secord Gated Spillway Demolition and Disposal Mechanical and Electrical Equipment Demolition and Disposal 250,000 4,250,000 Subtotal Left Embankment Repair and Stabilization (L = 470 feet Sheet Pile Cutoffs 90 \$
30 \$
40 \$
80 \$
80 \$
45 \$
35 \$ 28.200 Embankment Fill 4,600 2.600 138,000 CY CY CY CY CY CY Embankment Fill Filler Sand and Drainage Stone Layers Upstream Riprap Protection Downstream Riprap Protection Bedding Stone Crest Gravel Topsoil, Seed and Temporary Erosion Protection 3.03 104.000 3,700 2,100 2,000 296,000 168,000 90,000 7,000 3.341.000 Right Embankment Repair and Stabilization (L = 360 feel
Sheet Pile Cutoffs
Embankment Fill
Embankment Fill
Filter Sand and Drainage Stone Layers
Upstream Riprap Protection
Downstream Riprap Protection
Bedding Stone
Crest Gravel
Topsoil, Seed and Temporary Erosion Protection 90 \$
30 \$
40 \$
80 \$
80 \$
45 \$
35 \$
2.00 \$
81 21,600 3,500 2,000 2,800 1,600 1,500 100 0 SF CY CY CY CY CY SY 2,552,000 New Gated Spillway and Outlet Works 5.00 6,724,000 1,200,000 667,000 1,296,000 New Gated spillway. Cost apportioned from Edenville Dam 6,724,000 \$ 400,000 \$ 667,000 \$ 120 \$ Secord 4-Bay Spillway Structure
Crest Gates (Shallow) - Installed with Hoists and Controls
Crest Gates (Deep) - Installed with Hoists and Controls
Sheet Pile Cutoffs EA EA SF EA 667,000 120 \$ 1,000,000 \$ 10,800 Subtotal 6.00 Powerhouse Rehabilitation Misc. surface concrete and masonry repairs
Convert water passages to low level outlet
Concrete Backfill
Foundation Micropiles and Structural Pile Caps Powerhouse rehabilitation costs removed. EA EA CY EA 200,000 \$ 500,000 \$ 6.01 6.02 6.03 600 \$ 20,000 \$ 6.04 Subtotal New 200 foot Labyrinth Spillway **7.00** 7.01 800 900 900 CY CY CY Increase spillway width from 125 feet to 200 feet 720,000 Reinforced Concrete Chute Slabs
Reinforced Concrete Stilling Basin Floor Slabs 7.02 800 \$ 800 \$ 720,000 7.03 720,000 7.04 Reinforced Concrete End Sill 128 CY 1.500 \$ 192.000 7.05 Reinforced Concrete Labyrinth Weir Walls 200 CY \$ 1,400 \$ 280 000 1,200 \$
90 \$
80 \$
80 \$
45 \$
35 \$
40 \$
25 \$ 7.06 7.07 Reinforced Concrete Spilllway and Stilling Basin Walls Steel Sheet Pile Cutoffs 400 480,000 CY SF CY CY CY CY LF LS 480,000 1,080,000 72,000 296,000 54,000 518,000 360,000 20,000 400 12,000 900 3,700 1,200 14,800 9,000 800 Upstream Riprap
Downstream Heavy Riprap Apron and Chute Bedding Structural Fill Filter Sand and Drainage Stone Drain Pipe (Solid and Slotted) 500,000 \$ Subtotal \$ Pre-Engineered Pedestrian Bridge and Piers (access over stilling basin) 5,512,000 Site Restoration Place Overburden, Seed, Fertilize, and Mulch Slopes Dam Safety Monitoring Instrumentation 100,000 30,000 130,000 36,847,000 Contingency
Construction Subtotal 11,054,000 47,901,000 7,185,000 Engineering Investigations, Design and Construction Engineering 15% Total Estimated Cost 55,086,000 say \$ Information presented on this sheet represents our opinion of probable costs in 2020 dollars. Unit and lump-sum prices are based on costs for similar projects, engineering judgment, and/or published cost data. Client administrative/engineering costs and regulatory fees not included. Actual bids and total project costs may vary based on contractor's perceived risk, site access, season, market conditions, etc. No warranties concerning the accuracy of costs presented herein are expressed or implied.

PINION OF PROBABLE COST - CONCEPTUAL